# Spiral-tube Heat Exchange in COMSOL

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# CLOSE-WOUND METAL COIL Axis-symmetric Core Convection Model

4" entrance turbulent jet

exit at an 8" orifice



solid conduction edge-region



# **Edge-Region Temperatures**



# Spiral Tube ID Model

distance along the coil, s

$$-A_f \frac{dp_f}{ds} = \tau_w P_f \quad \text{or} \quad \frac{dp_f}{ds} = -4\tau_w / D_H$$
$$\tau_w = (\frac{1}{2})\rho_f U_f^2 C_f \quad C_f = r_{cs} 0.046 / Re_f^{0.2}$$
$$r_{cs} = 1 + 0.11 Re_f^{0.23} (D_H / D_C)^{0.14} \approx 2.0$$

heat balance yields

$$\frac{d(mc_p T)_f}{ds} = q_w P_f \quad \text{or} \quad mc_p \frac{dT_f}{ds} = q_w \pi D_H$$
wall heat flux  $q_w = h_f (T_w - T_f)$ 
heat transfer coefficient is given by Reynold's analogy

$$h_f / (\rho C_p U)_f \equiv St \approx \frac{C_f}{2} P r^{-2/3}$$

## **Axial Tube ID Integration**

 $s = (\pi D_{c}/P)x \text{ ; therefore } d/ds = P/(\pi D_{c})d/dx$   $\frac{P}{\pi D_{c}}\frac{dp_{f}}{dx} = -4\tau_{w}/D_{H} \qquad \dot{m}C_{p}\frac{P}{\pi D_{c}}\frac{dT_{f}}{dx} = q_{w}\pi D_{H}$   $S_{f} = p_{f}/p_{fin} \qquad R_{f} = T_{f}/T_{fin}$   $P\frac{dS_{f}}{dx} = -4\pi(\tau_{w}/p_{fin})D_{c}/D_{H} \qquad P\frac{dR_{f}}{dx} = \pi^{2}q_{w}D_{c}D_{H}/\dot{m}C_{p}T_{fin}$ 





Determine effective conductivity, k<sub>s</sub> so the left-most temperatures are equal.



#### **Tube Wall and Fluid Temperatures**





## **OPEN-WOUND QUARTZ COIL**



#### **Radiation Properties**







#### heat loss coefficient

# heater temperature coefficient





## CONCLUSION

- Coil Heat Exchangers with different length scales and processes were modeled with COMSOL; shape factors linked processes into a unified model.
- *Combustion Example*: core turbulent convection and radiation heat transfer were linked to the spiral flow.
- *Electric-heater Example*: complex radiation to bank of tubes was simplified to an overall heat transfer coefficient.