COMSOL CONFERENCE 2015 BOSTON

COMSOL Conference 2015 Boston

Session: Optimization and Simulation Methods

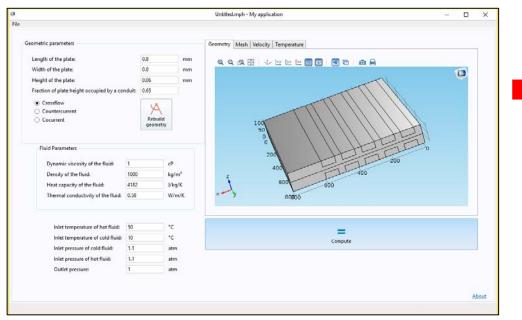


Session Chair: Jeffrey Fong, National Institute of Standards & Technology

October 8, 2015

1:00 PM - 2:30 PM

Application of COMSOL Multiphysics[™] Software in Transport Phenomena Educational Processes



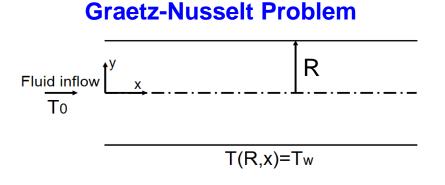
Mikhail Vasilev Pranav Sharma Patrick L. Mills*

Department of Chemical and Natural Gas Engineering Texas A & M University-Kingsville Kingsville-TX 78363-8202 USA *Patrick.Mills@tamuk.edu

> Anuradha Nagaraj Department of Environmental Engineering

Micro Heat Exchanger (MHE) Application

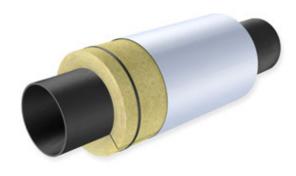
Transport Phenomena: Connecting Theory to Practical Problems



Not constant boundary conditions? Flux specified only for some region of the pipe? Imperfect thermal insulation?

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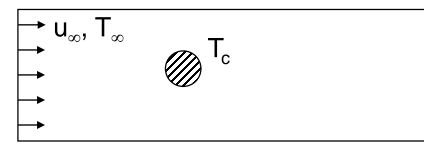
Electrically Heated Pipe



Subsea Pipeline



Nonisothermal Flow Over a Cylinder

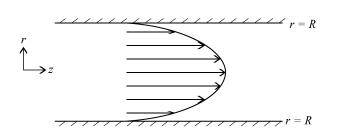


Complex arrangement of multiple pipes? Viscous flow? Higher Reynolds number?

Momentum transport

1-D fluid flow through a circular pipe

$$u(r) = u_{max} \left[1 - \left(\frac{r}{R}\right)^2 \right]$$



Energy transport

Linear heat conduction through a solid wall

$$T(x) = \frac{(T_2 - T_1)}{L}x + T_1$$

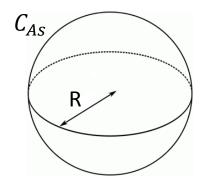
$$T_2$$

Mass transport

Fickian diffusion in isothermal spherical catalyst particle followed by a 1st order reaction.

$$\Psi(\lambda) = \frac{1}{\lambda} \left(\frac{\sinh(\phi\lambda)}{\sinh(\phi)} \right),$$

where $\Psi = \frac{C_A}{C_{As}}$ and $\lambda = \frac{r}{R}$



Pros:

 Not very complicated – Straightforward to understand

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- Existence of analytical solutions
- Provides initial insight into more complex problems

Cons:

- Lack of model response visualization
- Limited applicability to real-world problems
- Transient solutions for 1-D problems are not simple to compute, *e.g.*, infinite series of complex Eigenfunctions and Eigenvalues

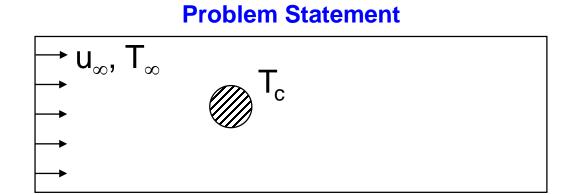
Desired Problem Attributes

- Reinforce 1-D problems by extension to multidimensions (2-D or 3-D) and multi-physics.
- Contains various physico-chemical parameters that can be varied by the user.
- Solution can be generated within seconds to minutes with modern computing hardware.
- Ability to readily modify the application to account ulletfor problem variations and other derived quantities.

Applications Developed

- Non-isothermal Flow Over a Cylinder
- Graetz-Nusselt Problem
- Flow Through a Duct
- Micro Heat Exchanger
- Rotating Cone Pump
- Catalytic Wall Microreactor
- T-Micromixer

Example 1: Nonisothermal Flow Over a Heated Cylinder



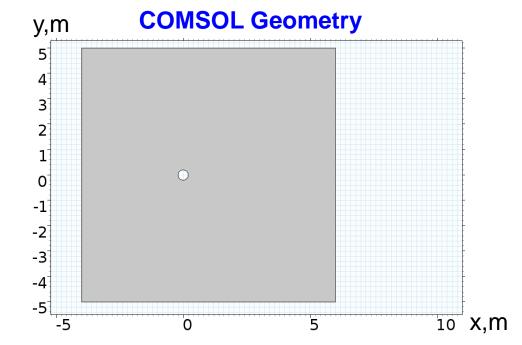
Model Equations

• Equation of Continuity

$$\nabla \cdot (\rho \boldsymbol{u}) = 0$$

- Navier-Stokes Equations $\rho(\boldsymbol{u} \cdot \nabla)\boldsymbol{u} = \nabla \cdot [p\boldsymbol{I} + \mu(\nabla \boldsymbol{u} + (\nabla \boldsymbol{u})^T)] + \boldsymbol{F}$
- Energy Transport Equations

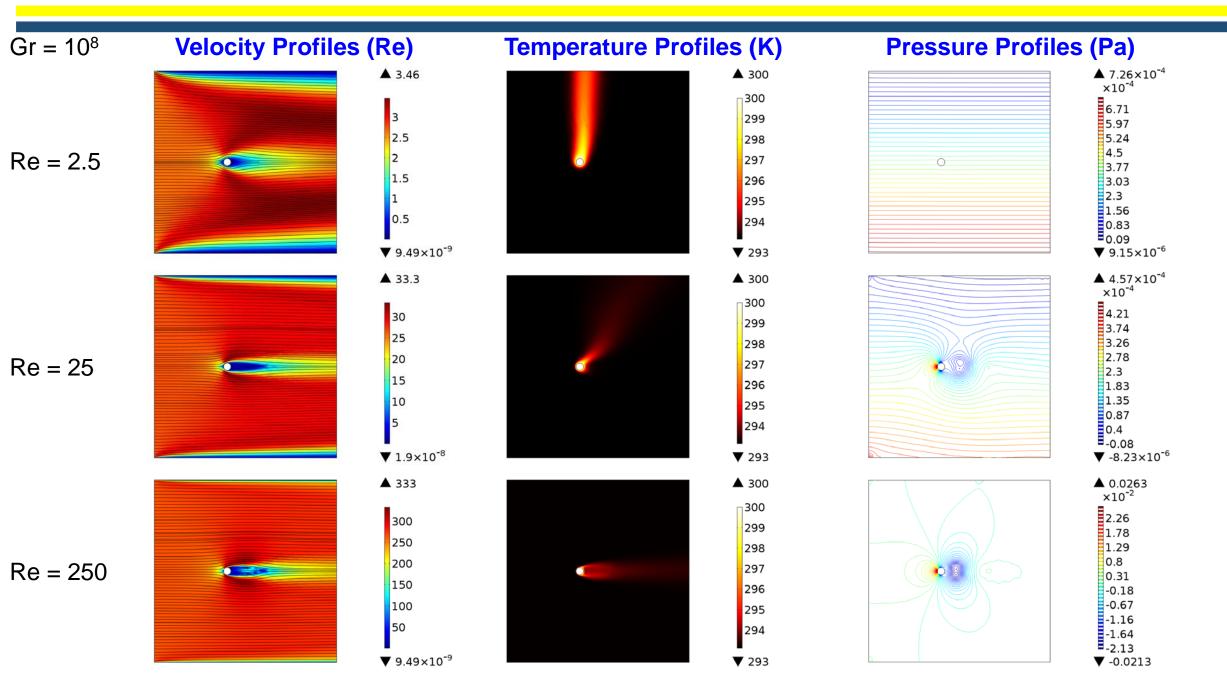
$$\rho C_p \boldsymbol{u} \cdot \nabla T + \nabla \cdot \boldsymbol{q} = Q + Q_{vd}$$
$$\boldsymbol{q} = -k\nabla T$$



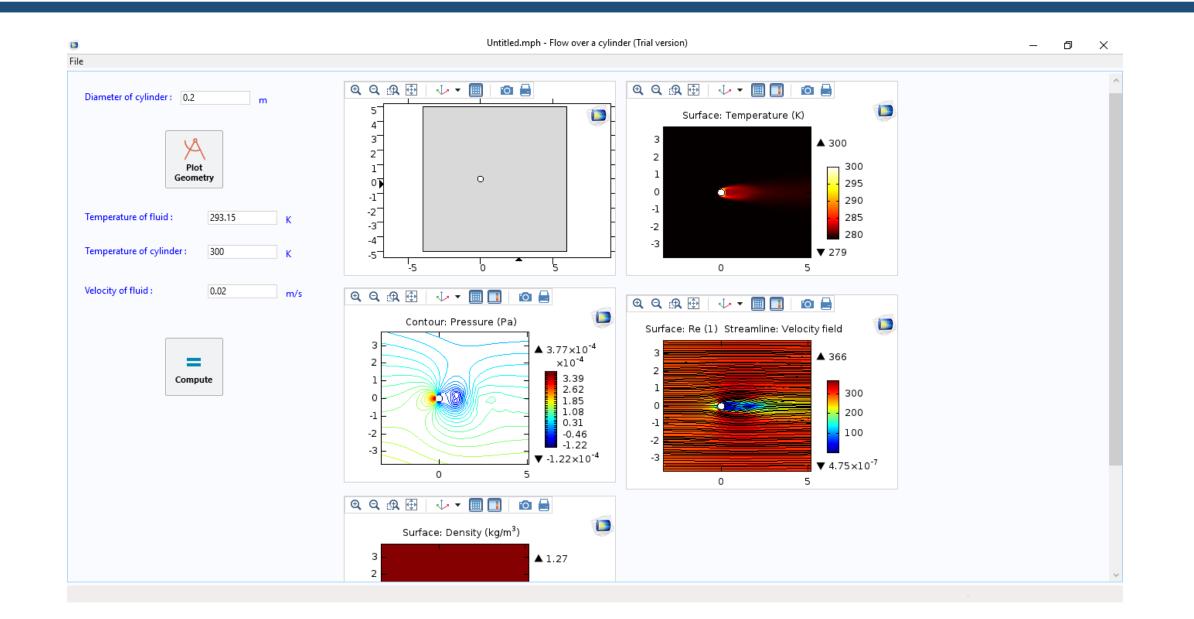
Model Parameters

** Name	Expression	Value	Description
Vinf	0.0002[m/s]	2E-4 m/s	Far-field velocity
Т0	300[K]	300 K	Temperature of the cylinder
T1	293.15[K]	293.15 K	Temperature of the fluid at the inlet
D	0.2[m]	0.2 m	Diameter of the cylinder
Н	10[m]	10 m	Height of the fluid domain

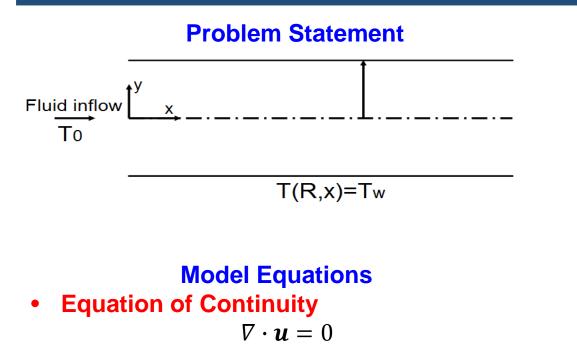
Velocity, Temperature and Pressure Profiles at Various Reynolds Numbers



COMSOL Application: Non-isothermal Flow over a Heated Cylinder

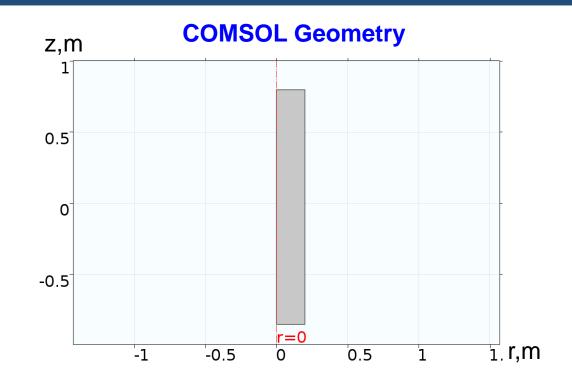


Example 2: Graetz-Nusselt Problem (Constant Wall Temperature)



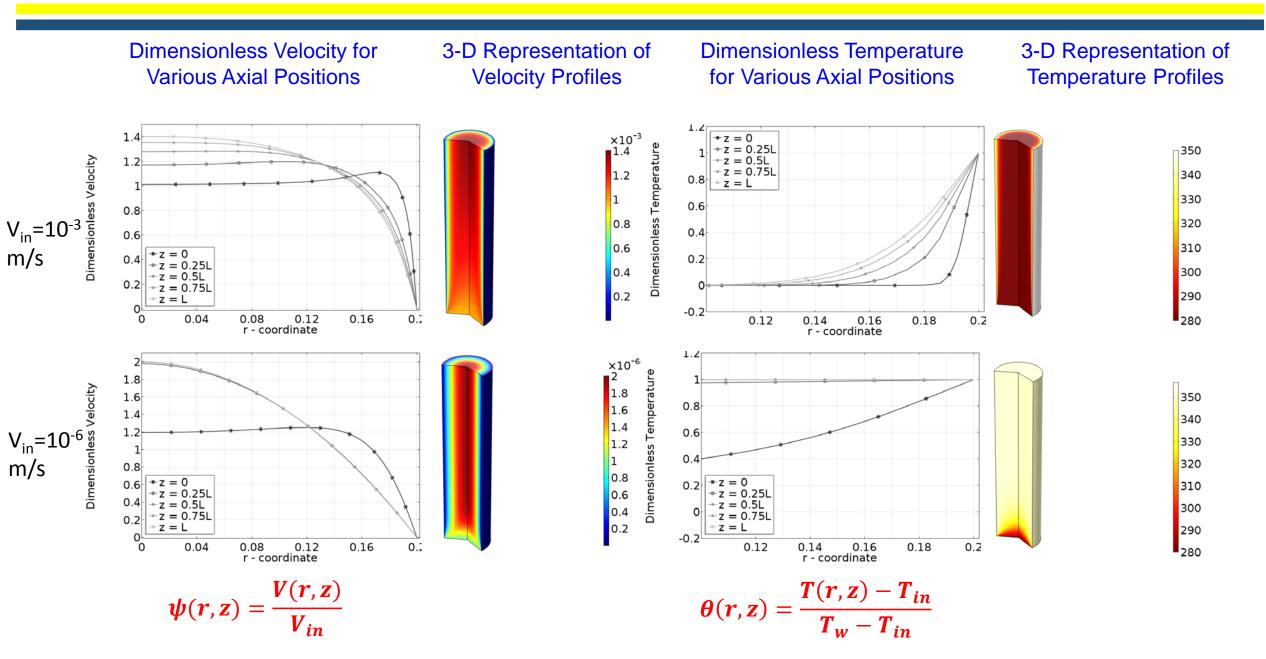
- Navier-Stokes Equations $\rho(\boldsymbol{u} \cdot \nabla)\boldsymbol{u} = \nabla \cdot [p\boldsymbol{I} + \mu(\nabla \boldsymbol{u} + (\nabla \boldsymbol{u})^T)] + F$
- Energy Transport Equations $\rho C_n \boldsymbol{u} \cdot \nabla T + \nabla \cdot \boldsymbol{q} = Q + Q$

$$C_p \boldsymbol{u} \cdot VT + V \cdot \boldsymbol{q} = Q + Q_{vd}$$
$$\boldsymbol{q} = -k\nabla T$$

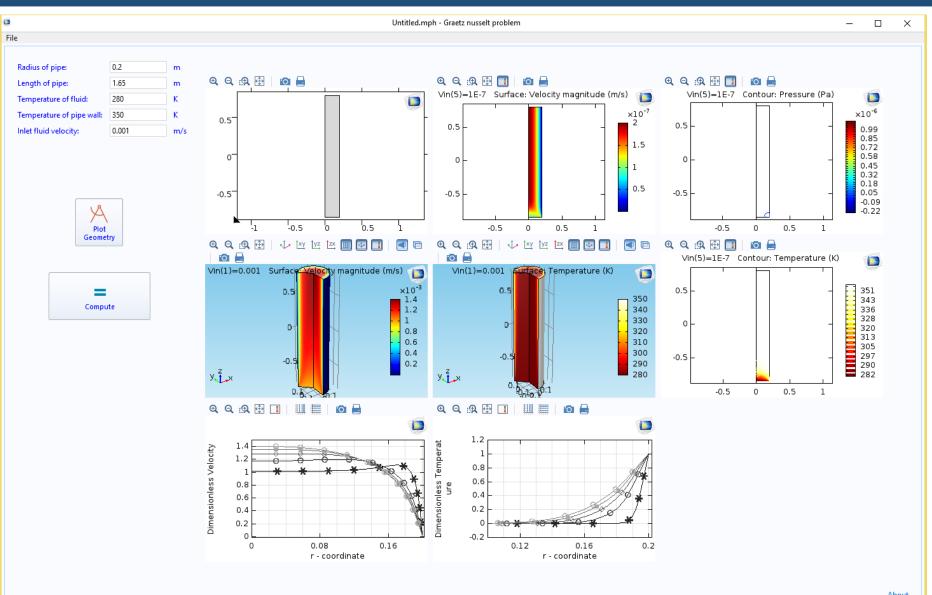


** Name	Expression	Value	Description
R	0.2[m]	0.2 m	Radius of pipe
L	1.65[m]	1.65 m	Length of pipe
Tin	280[K]	280 K	Temperature of fluid
Tw	350[K]	350 K	Temperature of pipe wall
Vin	0.001[m/s]	0.001 m/s	Inlet fluid velocity

Velocity and Temperature Profiles



COMSOL Application: Graetz-Nusselt Problem



Example 3: Micro Heat Exchanger

Objectives:

- Compare the heat exchanger effectiveness factor by changing the fluid flow.
- Predict temperature profiles by solving the coupled momentum-energy transport equations for a 3-D geometry.

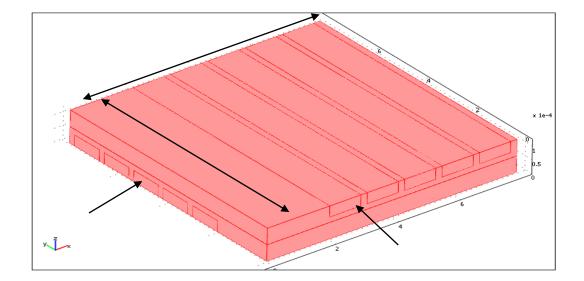
Model Geometry:

5 rectangular ducts

Cross-flow orientation

Dimensions:

Length of each slab Width of each slab Height of each slab No. of Microchannels Microchannel width Microchannel height Mat'l of Construction 800 μm 800 μm 60 μm 5 100 μm 30 μm Copper



Micro Heat Exchanger Model Equations & Effectiveness Factor

Model Equations:

Momentum Transport Equations

$$x- \text{ direction:} \qquad \rho \left[\frac{\partial u_x}{\partial t} \right] - \mu \left[\frac{\partial^2 u_x}{\partial x^2} + \frac{\partial^2 u_x}{\partial y^2} + \frac{\partial^2 u_x}{\partial z^2} \right] + \rho \left[u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_y}{\partial y} + u_z \frac{\partial u_z}{\partial z} \right] + \frac{\partial p}{\partial x} = 0$$

$$y-\text{direction:} \qquad \rho \left[\frac{\partial u_y}{\partial t} \right] - \mu \left[\frac{\partial^2 u_y}{\partial x^2} + \frac{\partial^2 u_y}{\partial y^2} + \frac{\partial^2 u_y}{\partial z^2} \right] + \rho \left[u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_y}{\partial y} + u_z \frac{\partial u_z}{\partial z} \right] + \frac{\partial p}{\partial y} = 0$$

$$z-\text{direction:} \qquad \rho \left[\frac{\partial u_z}{\partial t} \right] - \mu \left[\frac{\partial^2 u_z}{\partial x^2} + \frac{\partial^2 u_z}{\partial y^2} + \frac{\partial^2 u_z}{\partial z^2} \right] + \rho \left[u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_y}{\partial y} + u_z \frac{\partial u_y}{\partial z} \right] + \frac{\partial p}{\partial z} = 0$$

Conduction-Convection Equation:

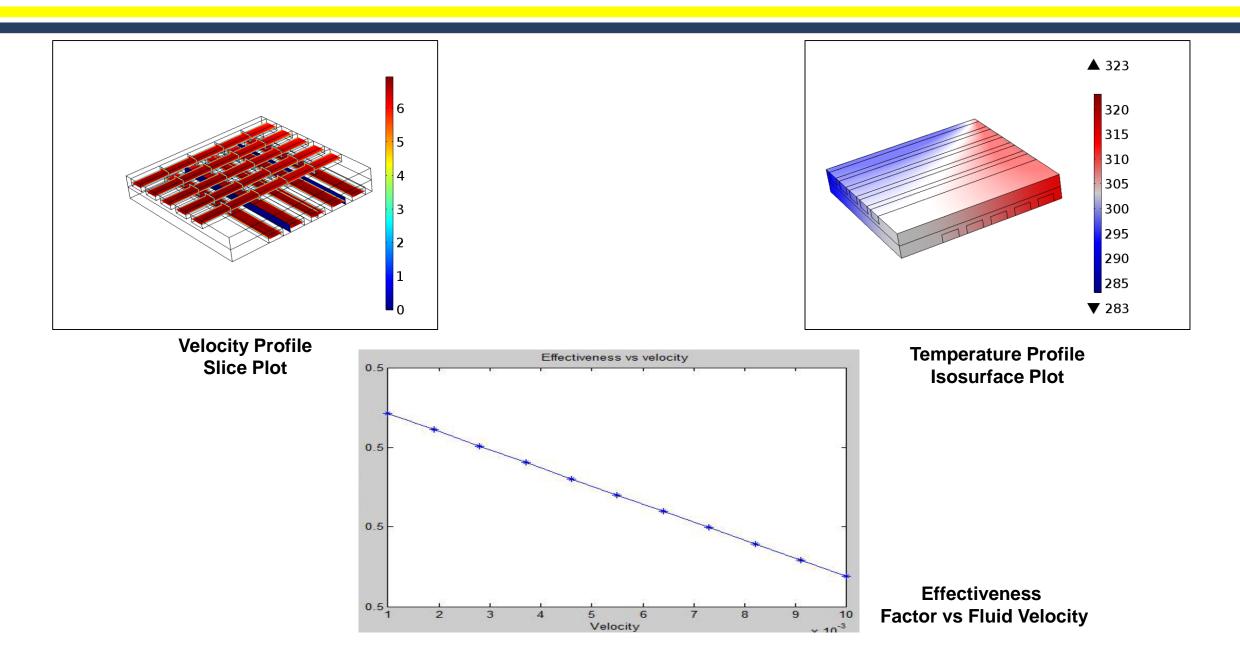
$$\rho C_p \left(\frac{\partial T}{\partial t} + u_x \frac{\partial T}{\partial x} + u_y \frac{\partial T}{\partial y} + u_z \frac{\partial T}{\partial z} \right) = \left(k_x \frac{\partial^2 T}{\partial x^2} + k_y \frac{\partial^2 T}{\partial y^2} + k_z \frac{\partial^2 T}{\partial z^2} \right) + Q$$

Parameter Estimation:

Effectiveness factor
$$\mathcal{E} = \frac{q}{q_{\text{max}}} = \frac{m^{\circ}C_{p}(T_{hot-in} - T_{hot-out})}{m^{\circ}C_{p}(T_{hot-in} - T_{cold-in})} = \frac{(T_{hot-in} - T_{hot-out})}{(T_{hot-in} - T_{cold-in})}$$

 ρ is the fluid density, η is the fluid viscosity, ρ is the fluid pressure, K is fluid conductivity, T is temperature, m° mass flow rate, and Cp is the Specific heat capacity

Micro Heat Exchanger Velocity & Temperature Profiles

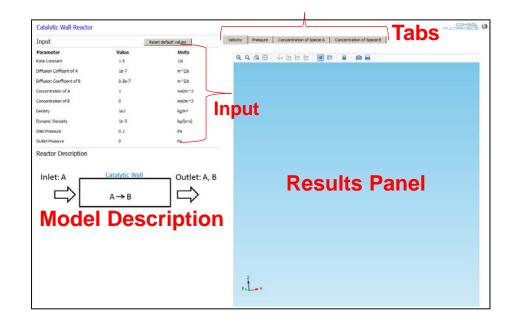


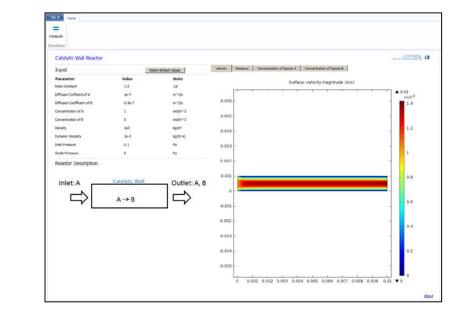
COMSOL Application: Micro Heat Exchanger

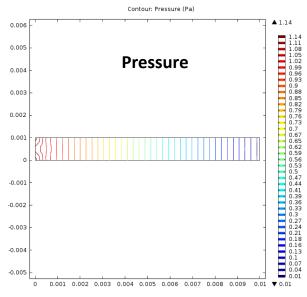
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File		
Geometric parameters		Geometry Mesh Velocity Temperature
Length of the plate: Width of the plate:	0.8 mm 0.8 mm	
Height of the plate: Fraction of plate height occupied by a co	0.06 mm	
 Crossflow Countercurrent Cocurrent 	Rebuild geometry	100 50 0
Fluid Parameters Dynamic viscosity of the fluid:	1 cP	200
Density of the fluid: Heat capacity of the fluid:	1000 kg/m ³ 4182 J/kg/K	400 2 600 600
Thermal conductivity of the fluid:		× • • • • 80800
Inlet temperature of hot fluid:	50 °C	
Inlet temperature of cold fluid:		=
Inlet pressure of cold fluid:	1.1 atm	Compute
Inlet pressure of hot fluid:	1.1 atm	
Outlet pressure:	1 atm	

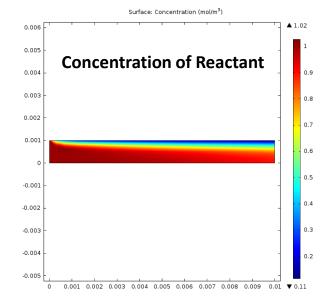
About

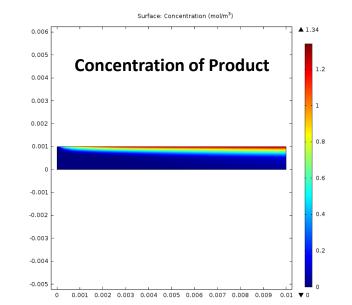
COMSOL Application: Catalytic Wall Microreactor



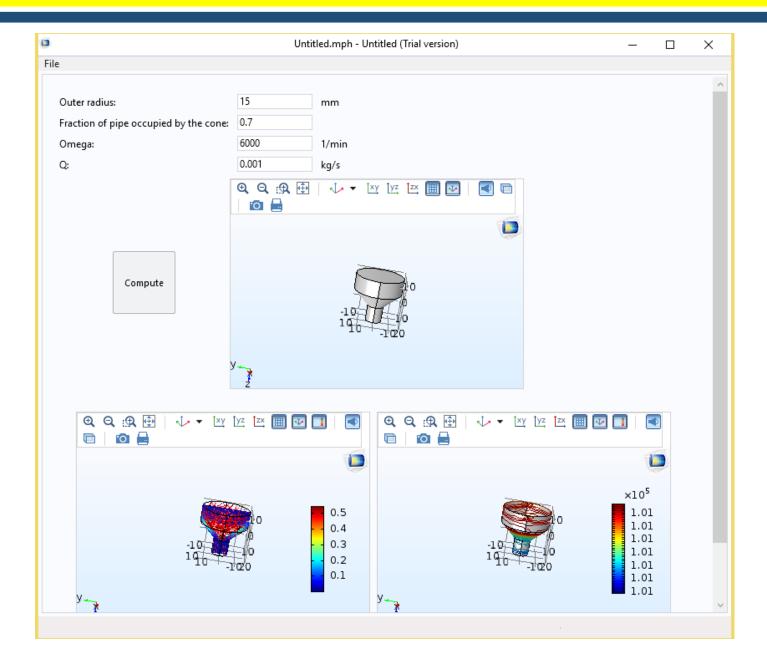








COMSOL Application: Rotating Cone Pump



Conclusions

COMSOL Multiphysics[™] :

- Provides robust representation of different multiphysics problems that can be used as a tool for teaching transport phenomena principles.
- Can be used as an intermediate learning instrument between university education and real-world applications.
- Allows different cases of the same problem to be combined into a single application for parametric studies.
- Allows more realistic simulation of real world problems for improved insight.

The student can observe the effect of input parameters on any output variable.

Thank you for your attention.