

## Solver Output

ANSYS Mechanical

```

-----
| W E L C O M E   T O   T H E   A N S Y S   P R O G R A M   |
|-----|

```

```

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```

```

***** ANSYS COMMAND LINE ARGUMENTS *****
BATCH MODE REQUESTED (-b) = NOLIST
INPUT FILE COPY MODE (-c) = COPY
2 PARALLEL CPUS REQUESTED
MEMORY REQUESTED (MB) = 96
START-UP FILE MODE = NOREAD
STOP FILE MODE = NOREAD
DATABASE SIZE REQUESTED (MB) = 32

00000000 VERSION=WINDOWS x64 RELEASE= 12.1 UP20091102
CURRENT JOBNAME=file 17:34:11 AUG 28, 2012 CP= 0.421

```

```
PARAMETER _DS_PROGRESS = 999.0000000
```

```
/INPUT FILE= ds.dat LINE= 0
```

```
DO NOT WRITE ELEMENT RESULTS INTO DATABASE
```

```
*GET _WALLSTRT FROM ACTI ITEM=TIME WALL VALUE= 17.5697222
```

```
TITLE=
Suction_pipe_28.08.2012--Modal (B5)
```

```
--- Data in consistent NMM units.
```

```
MPA UNITS SPECIFIED FOR INTERNAL
LENGTH = MILLIMETERS (mm)
MASS = TONNE (Mg)
TIME = SECONDS (sec)
TEMPERATURE = CELSIUS (C)
TOFFSET = 273.0
FORCE = NEWTON (N)
HEAT = MILLIJOULES (mJ)

```

```
INPUT UNITS ARE ALSO SET TO MPA
```

```
*****TRACK MONITOR LEVEL= -1
TRACK PRINT LEVEL = 0
TRACK SUMMARY LEVEL= 0
```

```
1
```

```
***** ANSYS - ENGINEERING ANALYSIS SYSTEM RELEASE 12.1 *****
ANSYS Mechanical
```

00000000 VERSION=WINDOWS x64 17:34:11 AUG 28, 2012 CP= 0.437

Suction\_pipe\_28.08.2012--Modal (B5)

```
***** ANSYS ANALYSIS DEFINITION (PREP7) *****
***** Nodes for the whole assembly *****
***** Elements for Body 1 "Surface Body" *****
***** Elements for Body 2 "Surface Body" *****
***** Send User Defined Coordinate System(s) *****
***** Set Reference Temperature *****
***** Send Materials *****
***** Send Sheet Properties *****
***** Create Contact "Contact Region" *****
***** Real Contact Set For Above Contact Is 4 3 *****
***** Fixed Supports *****
```

\*\*\*\*\* ROUTINE COMPLETED \*\*\*\*\* CP = 0.515

```
--- Number of total nodes = 6027
--- Number of contact elements = 416
--- Number of spring elements = 0
--- Number of solid elements = 5976
--- Number of total elements = 6392
```

\*GET \_WALLBSOL FROM ACTI ITEM=TIME WALL VALUE= 17.5697222

\*\*\*\*\* ANSYS SOLUTION ROUTINE \*\*\*\*\*

PERFORM A MODAL ANALYSIS  
THIS WILL BE A NEW ANALYSIS

USE SYM. BLOCK LANCZOS MODE E TRACTION METHOD  
E TRACT 10 MODES  
NORMALIZE THE MODE SHAPES TO THE MASS MATRI

ERASE THE CURRENT DATABASE OUTPUT CONTROL TABLE.

WRITE ALL ITEMS TO THE DATABASE WITH A FREQUENCY OF NONE  
FOR ALL APPLICABLE ENTITIES

WRITE NSOL ITEMS TO THE DATABASE WITH A FREQUENCY OF ALL  
FOR ALL APPLICABLE ENTITIES

PRINTOUT RESUMED BY /GOP

E PAND ALL E TRACTED MODES  
DO NOT CALCULATE ELEMENT RESULTS

\*GET ANSINTER\_ FROM ACTI ITEM=INT VALUE= 0.00000000

```
*IF ANSINTER_ ( = 0.00000 ) NE
0 ( = 0.00000 ) THEN
```

\*ENDIF

\*\*\*\*\* ANSYS SOLVE COMMAND \*\*\*\*\*

\*\*\* WARNING \*\*\* CP = 0.515 TIME= 17:34:11  
Element shape checking is currently inactive. Issue SHPP,ON or  
SHPP,WARN to reactivate, if desired.

\*\*\* NOTE \*\*\* CP = 0.546 TIME= 17:34:11  
The model data was checked and warning messages were found.  
Please review output or errors file ( D: FEA\_2012-13 OPTYMA-  
MIZ015 FEA\_ProjectScratch ScrC758 file.err ) for these warning  
messages.

\*\*\* SELECTION OF ELEMENT TECHNOLOGIES FOR APPLICABLE ELEMENTS \*\*\*  
--- GIVE SUGGESTIONS AND RESET THE KEY OPTIONS ---

ELEMENT TYPE 1 IS SHELL181. IT IS ASSOCIATED WITH ELASTOPLASTIC  
MATERIALS ONLY. KEYOPT(8)=2 IS SUGGESTED AND KEYOPT(3)=2 IS SUGGESTED FOR  
HIGHER ACCURACY OF MEMBRANE STRESSES OTHERWISE, KEYOPT(3)=0 IS SUGGESTED.  
KEYOPT(8) HAS BEEN RESET BUT KEYOPT(3) CAN NOT BE RESET HERE. PLEASE RESET  
IT MANUALLY IF NECESSARY.

KEYOPT(1-12)= 0 0 2 0 0 0 0 2 0 0 0 0

ELEMENT TYPE 1 HAS KEYOPT(3)=2. FOR THE SPECIFIED ANALYSIS TYPE, LUMPED MASS  
MATRI OPTION (LUMPM, ON) IS SUGGESTED.

ELEMENT TYPE 2 IS SHELL181. IT IS ASSOCIATED WITH ELASTOPLASTIC  
MATERIALS ONLY. KEYOPT(8)=2 IS SUGGESTED AND KEYOPT(3)=2 IS SUGGESTED FOR  
HIGHER ACCURACY OF MEMBRANE STRESSES OTHERWISE, KEYOPT(3)=0 IS SUGGESTED.  
KEYOPT(8) HAS BEEN RESET BUT KEYOPT(3) CAN NOT BE RESET HERE. PLEASE RESET  
IT MANUALLY IF NECESSARY.

KEYOPT(1-12)= 0 0 2 0 0 0 0 2 0 0 0 0

ELEMENT TYPE 2 HAS KEYOPT(3)=2. FOR THE SPECIFIED ANALYSIS TYPE, LUMPED MASS  
MATRI OPTION (LUMPM, ON) IS SUGGESTED.

1

\*\*\*\*\* ANSYS - ENGINEERING ANALYSIS SYSTEM RELEASE 12.1 \*\*\*\*\*  
ANSYS Mechanical  
00000000 VERSION=WINDOWS x64 17:34:11 AUG 28, 2012 CP= 0.577

Suction\_pipe\_28.08.2012--Modal (B5)

S O L U T I O N O P T I O N S

PROBLEM DIMENSIONALITY. . . . .3-D  
DEGREES OF FREEDOM. . . . . U UY UZ ROT ROTY ROTZ

```

ANALYSIS TYPE . . . . .MODAL
E TRACTION METHOD. . . . .BLOCK LANCZOS
NUMBER OF MODES TO E TRACT. . . . . 10
GLOBALLY ASSEMBLED MATRI . . . . .SYMMETRIC
NUMBER OF MODES TO E PAND . . . . .ALL
ELEMENT RESULTS CALCULATION . . . . .OFF

*** WARNING ***                CP =      0.608   TIME= 17:34:11
Material number 4 (used by element 5977 ) should normally have at least
one MP or one TB type command associated with it.  Output of energy by
material may not be available.

*** NOTE ***                    CP =      0.608   TIME= 17:34:11
The step data was checked and warning messages were found.
Please review output or errors file ( D: FEA_2012-13 OPTYMA-
MIZ015 FEA _ProjectScratch ScrC758 file.err ) for these warning
messages.

*** NOTE ***                    CP =      0.608   TIME= 17:34:11
The conditions for direct assembly have been met.  No .emat or .erot
files will be produced.

      L O A D   S T E P   O P T I O N S

LOAD STEP NUMBER. . . . . 1
PRINT OUTPUT CONTROLS . . . . .NO PRINTOUT
DATABASE OUTPUT CONTROLS
ITEM      FREQUENCY  COMPONENT
ALL       NONE
NSOL     ALL

*** NOTE ***                    CP =      0.733   TIME= 17:34:11
Symmetric Deformable- deformable contact pair identified by real
constant set 3 and contact element type 3 has been set up.  The
companion pair has real constant set ID 4.  Both pairs should have the
same behavior.
For asymmetric contact analysis, you may deactivate the current pair
and keep its companion pair.
Contact algorithm: Penalty method
Contact detection at: Gauss integration point
Contact stiffness factor FKN          10.000
The resulting contact stiffness      0.59278E 06
Default penetration tolerance factor FTOLN 0.10000
The resulting penetration tolerance   0.36000
Default opening contact stiffness OPSF will be used.
Default tangent stiffness factor FKT   1.0000
Default Max. friction stress TAUMA    0.10000E 21
Average contact surface length        2.9468
Average contact pair depth            3.6000
User defined pinball region PINB     0.97924
Initial penetration/gap is excluded.
Bonded contact (always) is defined.

*** NOTE ***                    CP =      0.733   TIME= 17:34:11
Min. Initial gap 0.566595164 was detected between contact element 6180
and target element 6353.
The gap is closed due to initial adjustment.

Max. Closed gap 0.664059952 has been detected between contact element
6092 and target element 6248.

*** WARNING ***                CP =      0.733   TIME= 17:34:11
The closed gap/penetration may be too large.  Increase pinball if it is
a true closed gap/penetration.  Decrease pinball if it is a false one.
*****

*** NOTE ***                    CP =      0.733   TIME= 17:34:11
Symmetric Deformable- deformable contact pair identified by real
constant set 4 and contact element type 3 has been set up.  The
companion pair has real constant set ID 3.  Both pairs should have the
same behavior.
For asymmetric contact analysis, you may keep the current pair and
deactivate its companion pair.
Contact algorithm: Penalty method
Contact detection at: Gauss integration point
Contact stiffness factor FKN          10.000
The resulting contact stiffness      0.59278E 06
Default penetration tolerance factor FTOLN 0.10000
The resulting penetration tolerance   0.38800
Default opening contact stiffness OPSF will be used.
Default tangent stiffness factor FKT   1.0000
Default Max. friction stress TAUMA    0.10000E 21
Average contact surface length        2.8237
Average contact pair depth            3.8800
User defined pinball region PINB     0.97924
Initial penetration/gap is excluded.
Bonded contact (always) is defined.

*** NOTE ***                    CP =      0.733   TIME= 17:34:11
Min. Initial gap 0.531614275 was detected between contact element 6207
and target element 5988.
The gap is closed due to initial adjustment.

Max. Closed gap 0.646968253 has been detected between contact element
6231 and target element 6017.

*** WARNING ***                CP =      0.733   TIME= 17:34:11
The closed gap/penetration may be too large.  Increase pinball if it is
a true closed gap/penetration.  Decrease pinball if it is a false one.
*****

**** CENTER OF MASS, MASS, AND MASS MOMENTS OF INERTIA ****

CALCULATIONS ASSUME ELEMENT MASS AT ELEMENT CENTROID

TOTAL MASS = 0.42886E-03

```

CENTER OF MASS	MOM. OF INERTIA ABOUT ORIGIN	MOM. OF INERTIA ABOUT CENTER OF MASS
C = -8.0314	I = 14.28	I = 6.633
YC = 126.83	IYY = 3.594	IYY = 2.814
ZC = 41.890	IZZ = 11.22	IZZ = 4.297
	I Y = 0.4759	I Y = 0.3903E-01
	IYZ = -2.321	IYZ = -0.4217E-01
	IZ = -0.3636E-01	IZ = -0.1806

\*\*\* MASS SUMMARY BY ELEMENT TYPE \*\*\*

TYPE	MASS
1	0.521739E-04
2	0.376685E-03

Range of element maximum matrix coefficients in global coordinates  
Maximum = 825945.175 at element 6228.  
Minimum = 45279.0232 at element 1252.

\*\*\* ELEMENT MATRI FORMULATION TIMES

TYPE	NUMBER	ENAME	TOTAL CP	AVE CP
1	774	SHELL181	0.125	0.000161
2	5202	SHELL181	0.546	0.000105
3	208	CONTA174	0.016	0.000075
4	208	TARGE170	0.000	0.000000

Time at end of element matrix formulation CP = 1.5132097.

BLOCK LANCZOS CALCULATION OF UP TO 10 EIGENVECTORS.  
NUMBER OF EQUATIONS = 32946  
MA IMUM WAVEFRONT = 126  
MA IMUM MODES STORED = 10  
MINIMUM EIGENVALUE = 0.00000E 00  
MA IMUM EIGENVALUE = 0.10000E 09

\*\*\* NOTE \*\*\* CP = 1.654 TIME= 17:34:12  
The initial memory allocation (-m) has been exceeded.  
Supplemental memory allocations are being used.  
Memory allocated for solver = 92.393 MB  
Memory required for in-core = 77.477 MB  
Optimal memory required for out-of-core = 41.941 MB  
Minimum memory required for out-of-core = 32.633 MB

\*\*\* NOTE \*\*\* CP = 1.810 TIME= 17:34:12  
The Block Lanczos solver is currently running in the in-core memory mode. This memory mode uses the most amount of memory in order to avoid using the hard drive as much as possible, which most often results in the fastest solution time. This mode is recommended if enough physical memory is present to accommodate all of the solver data.

LANCZOS CYCLE NUMBER = 1

new shift: 8.4724D 03 modes still needed: 10

FREQUENCIES AT CURRENT LANCZOS CYCLE

1	0.18269791E 04	2	0.16925433E 04	3	0.16741231E 04
4	0.16343635E 04	5	0.10633885E 04	6	0.93045236E 03
7	0.79484812E 03	8	0.58976161E 03	9	0.37365736E 03
10	0.24948864E 03	11	0.22670871E 03	12	0.13926136E 03
13	0.98479065E 02				

number of steps : 7  
eigenvalues found : 13  
total no. eigenvalues: 13

LANCZOS CYCLE NUMBER = 2

new shift: 1.0805D 08 modes still needed: 0

1

\*\*\*\*\* ANSYS - ENGINEERING ANALYSIS SYSTEM RELEASE 12.1 \*\*\*\*\*  
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00000000 VERSION=WINDOWS x64 17:34:13 AUG 28, 2012 CP= 3.900

Suction\_pipe\_28.08.2012--Modal (B5)

\*\*\* FREQUENCIES FROM BLOCK LANCZOS ITERATION \*\*\*

MODE	FREQUENCY (HERTZ)
------	-------------------

1	98.47906502492
2	139.2613589560
3	226.7087055536
4	249.4886383987
5	373.6573631023
6	589.7616080792
7	794.8481190824
8	930.4523567253
9	1063.388505478
10	1634.363532720

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\*\*\*\*\* ANSYS - ENGINEERING ANALYSIS SYSTEM RELEASE 12.1 \*\*\*\*\*  
ANSYS Mechanical  
00000000 VERSION=WINDOWS x64 17:34:13 AUG 28, 2012 CP= 4.056

Suction\_pipe\_28.08.2012--Modal (B5)

\*\*\*\*\* PARTICIPATION FACTOR CALCULATION \*\*\*\*\* DIRECTION

MODE	FREQUENCY	PERIOD	PARTIC.FACTOR	RATIO	EFFECTIVE MASS	CUMULATIVE MASS FRACTION	RATIO EFF.MASS TO TOTAL MASS
------	-----------	--------	---------------	-------	----------------	-----------------------------	---------------------------------

1	98.4791	0.10154E-01	0.14176E-01	1.000000	0.200967E-03	0.654381	0.468608	
2	139.261	0.71807E-02	0.33742E-02	0.238014	0.113849E-04	0.691452	0.265469E-01	
3	226.709	0.44109E-02	-0.18414E-02	0.129893	0.339078E-05	0.702493	0.790650E-02	
4	249.489	0.40082E-02	0.10944E-02	0.077197	0.119764E-05	0.706392	0.279262E-02	
5	373.657	0.26762E-02	0.80148E-02	0.565368	0.642372E-04	0.915559	0.149786	
6	589.762	0.16956E-02	0.36237E-02	0.255618	0.131313E-04	0.958316	0.306192E-01	
7	794.848	0.12581E-02	-0.18892E-03	0.013327	0.356918E-07	0.958433	0.832250E-04	
8	930.452	0.10747E-02	0.88839E-03	0.062668	0.789242E-06	0.961003	0.184033E-02	
9	1063.39	0.94039E-03	0.27263E-02	0.192315	0.743276E-05	0.985205	0.173315E-01	
10	1634.36	0.61186E-03	-0.21316E-02	0.150364	0.454374E-05	1.00000	0.105950E-01	
sum							0.307110E-03	0.716110

\*\*\*\*\* PARTICIPATION FACTOR CALCULATION \*\*\*\*\* Y DIRECTION

MODE	FREQUENCY	PERIOD	PARTIC.FACTOR	RATIO	EFFECTIVE MASS	CUMULATIVE MASS FRACTION	RATIO EFF.MASS TO TOTAL MASS
1	98.4791	0.10154E-01	0.15552E-03	0.013683	0.241851E-07	0.722022E-04	0.563939E-04
2	139.261	0.71807E-02	-0.96211E-02	0.846499	0.925650E-04	0.276417	0.215840
3	226.709	0.44109E-02	-0.68406E-02	0.601861	0.467936E-04	0.416115	0.109112
4	249.489	0.40082E-02	0.11366E-01	1.000000	0.129180E-03	0.801769	0.301217
5	373.657	0.26762E-02	-0.27460E-02	0.241599	0.754026E-05	0.824279	0.175821E-01
6	589.762	0.16956E-02	0.64689E-02	0.569162	0.418472E-04	0.949210	0.975778E-01
7	794.848	0.12581E-02	0.32792E-02	0.288520	0.107534E-04	0.981314	0.250745E-01
8	930.452	0.10747E-02	0.24558E-02	0.216069	0.603086E-05	0.999318	0.140626E-01
9	1063.39	0.94039E-03	-0.47648E-03	0.041923	0.227035E-06	0.999996	0.529393E-03
10	1634.36	0.61186E-03	-0.36500E-04	0.003211	0.133227E-08	1.00000	0.310654E-05
sum					0.334963E-03		0.781055

\*\*\*\*\* PARTICIPATION FACTOR CALCULATION \*\*\*\*\* Z DIRECTION

MODE	FREQUENCY	PERIOD	PARTIC.FACTOR	RATIO	EFFECTIVE MASS	CUMULATIVE MASS FRACTION	RATIO EFF.MASS TO TOTAL MASS
1	98.4791	0.10154E-01	-0.30691E-02	0.285234	0.941967E-05	0.369772E-01	0.219645E-01
2	139.261	0.71807E-02	0.10760E-01	1.000000	0.115780E-03	0.491477	0.269973
3	226.709	0.44109E-02	-0.36161E-02	0.336065	0.130762E-04	0.542808	0.304906E-01
4	249.489	0.40082E-02	0.86759E-02	0.806305	0.752720E-04	0.838291	0.175517
5	373.657	0.26762E-02	0.11494E-02	0.106825	0.132123E-05	0.843477	0.308081E-02
6	589.762	0.16956E-02	-0.28579E-02	0.265598	0.816739E-05	0.875539	0.190445E-01
7	794.848	0.12581E-02	0.39753E-03	0.036945	0.158031E-06	0.876159	0.368492E-03
8	930.452	0.10747E-02	0.38750E-02	0.360123	0.150153E-04	0.935102	0.350123E-01
9	1063.39	0.94039E-03	0.38252E-02	0.355498	0.146322E-04	0.992541	0.341188E-01
10	1634.36	0.61186E-03	0.13784E-02	0.128105	0.190005E-05	1.00000	0.443047E-02
sum					0.254742E-03		0.594000

\*\*\*\*\* PARTICIPATION FACTOR CALCULATION \*\*\*\*\* ROT DIRECTION

MODE	FREQUENCY	PERIOD	PARTIC.FACTOR	RATIO	EFFECTIVE MASS	CUMULATIVE MASS FRACTION
1	98.4791	0.10154E-01	-0.80788	0.238191	0.652673	0.492294E-01
2	139.261	0.71807E-02	3.3917	1.000000	11.5039	0.916941
3	226.709	0.44109E-02	-0.51548	0.151979	0.265715	0.936983
4	249.489	0.40082E-02	0.71070	0.209537	0.505089	0.975081
5	373.657	0.26762E-02	-0.10176	0.030003	0.103556E-01	0.975862
6	589.762	0.16956E-02	0.16790	0.049501	0.281888E-01	0.977988
7	794.848	0.12581E-02	-0.34723	0.102376	0.120570	0.987082
8	930.452	0.10747E-02	0.19833	0.058473	0.393331E-01	0.990049
9	1063.39	0.94039E-03	0.36293	0.107003	0.131715	0.999984
10	1634.36	0.61186E-03	0.14611E-01	0.004308	0.213475E-03	1.00000
sum					13.2578	

\*\*\*\*\* PARTICIPATION FACTOR CALCULATION \*\*\*\*\* ROTY DIRECTION

MODE	FREQUENCY	PERIOD	PARTIC.FACTOR	RATIO	EFFECTIVE MASS	CUMULATIVE MASS FRACTION
1	98.4791	0.10154E-01	1.3589	1.000000	1.84665	0.601224
2	139.261	0.71807E-02	0.22759	0.167476	0.517955E-01	0.618088
3	226.709	0.44109E-02	-1.0119	0.744630	1.02392	0.951451
4	249.489	0.40082E-02	-0.31640	0.232835	0.100111	0.984045
5	373.657	0.26762E-02	0.15235	0.112115	0.232120E-01	0.991602
6	589.762	0.16956E-02	-0.83385E-01	0.061361	0.695307E-02	0.993866
7	794.848	0.12581E-02	0.82437E-02	0.006066	0.679593E-04	0.993888
8	930.452	0.10747E-02	-0.88295E-01	0.064975	0.779607E-02	0.996426
9	1063.39	0.94039E-03	0.93402E-01	0.068733	0.872387E-02	0.999267
10	1634.36	0.61186E-03	0.47462E-01	0.034926	0.225263E-02	1.00000
sum					3.07148	

\*\*\*\*\* PARTICIPATION FACTOR CALCULATION \*\*\*\*\* ROTZ DIRECTION

MODE	FREQUENCY	PERIOD	PARTIC.FACTOR	RATIO	EFFECTIVE MASS	CUMULATIVE MASS FRACTION
1	98.4791	0.10154E-01	-2.6623	1.000000	7.08791	0.727693
2	139.261	0.71807E-02	-0.66569	0.250041	0.443141	0.773189
3	226.709	0.44109E-02	-0.90067	0.338303	0.811204	0.856473
4	249.489	0.40082E-02	-0.78481	0.294784	0.615923	0.919708
5	373.657	0.26762E-02	-0.39573	0.148642	0.156604	0.935786
6	589.762	0.16956E-02	-0.61953	0.232702	0.383812	0.975190
7	794.848	0.12581E-02	0.11973	0.044974	0.143364E-01	0.976662
8	930.452	0.10747E-02	-0.42336	0.159020	0.179235	0.995064
9	1063.39	0.94039E-03	-0.23111E-01	0.008681	0.534096E-03	0.995119
10	1634.36	0.61186E-03	0.21805	0.081903	0.475462E-01	1.00000



```
| Maximum Scratch Memory Used      =    27317732 Words    104.209 MB |  
|-----|  
| CP Time      (sec) =          4.072      Time = 17:34:14 |  
| Elapsed Time (sec) =          7.000      Date  = 08/28/2012 |  
|-----|
```