



# Numerical Modeling of 3D Electrowetting Droplet Actuation and Cooling of a Hotspot

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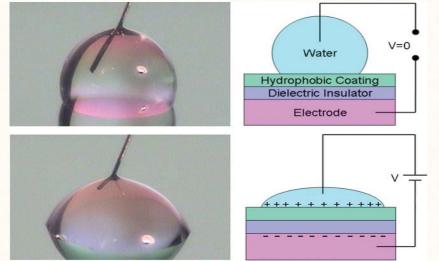
**University of Texas at Arlington** 



## What is EWOD?

- A micro-scale fluidic phenomena that can be used to manipulate liquid droplets
- Manipulation of liquid by modifying the surface properties by applying voltage





#### Lippman-young equation:

$$Cos\theta(V) = Cos\theta(0) + \frac{C_d}{2\gamma}V^2$$

**Top:** A water drop placed on a hydrophobic surface with a high contact angle. **Bottom:** Electrowetting of the surface. [Ref. Shamai et al.]

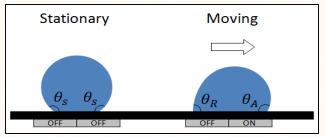


## What is EWOD actuation?

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#### **Open configuration**



 By Creating asymmetric contact angle around meniscus, net pressure difference can be created and droplet can move [2]

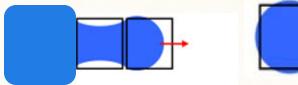
#### Parallel plate EWOD device

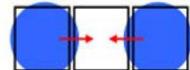
- Less sample volume
- Less contamination
- Faster reaction
- Flexible
- Portable

#### **Basic operations**

Top view

Droplet generation **Droplet Merging** 

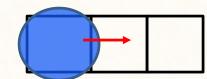




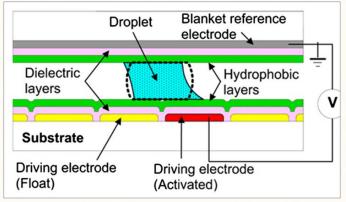
**Droplet Splitting** 







Cross-sectional view



Ref. Hsien-Hua et al.

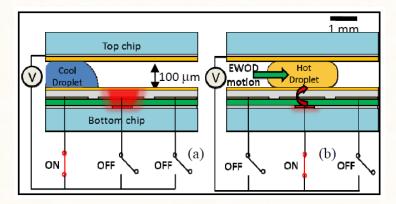


# Objectives & Motivation



#### Objectives

- Modeling coupled physics:
- Droplet motion + Cooling of a hotspot (Fluid flow) (Heat transfer)
- Comparing results from numerical modeling with experiments



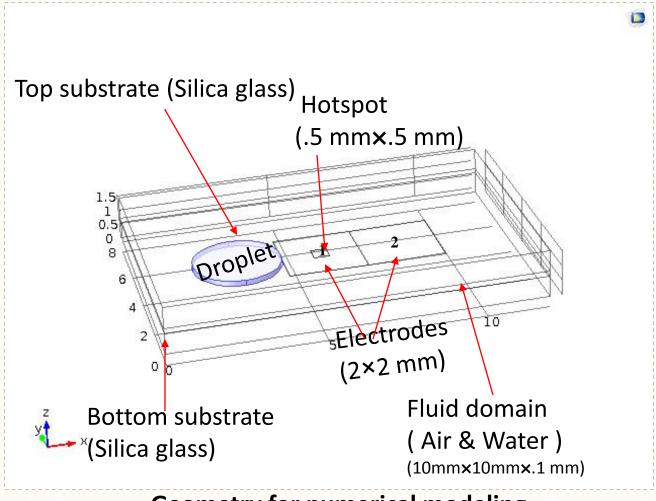
**Cross-section of DMF Cooling Chip** 

- Motivation
- Understanding the physics
  - Overcome challenges in experiments
    - Parametric study of geometric dimensions
      - Complicated EWOD fabrication
- Easy approximate temperature measurement
- Parametric study for optimum heat transfer performance



# Model Description







## Numerical Formulations



#### • Governing equations:

- Incompressible, constant properties flow
- Navier-stokes equations:

$$\nabla \cdot \boldsymbol{u} = 0$$
 shear and air drag actuating force 
$$\rho \left( \frac{\partial \boldsymbol{u}}{\partial t} + \boldsymbol{u} \cdot \nabla \boldsymbol{u} \right) + \nabla p - \mu \nabla^2 \boldsymbol{u} = F_{\text{st}}$$

$$\mathbf{F}_{st} = \sigma k \delta(\phi) \nabla \phi$$

k=curvature of the interface  $\sigma$ =surface tension.

 $\delta$ =Dirac delta function (only non-zero at the interface

Φ=Phase field variable

#### • Energy equation:

$$\rho \text{Cp.}\mathbf{u}.\nabla T + \rho \text{Cp.}\partial T/\partial t = \nabla.(K\nabla T)$$

C<sub>p</sub>=Specific heat capacity ρ=Density K=Thermal conductivity





- Use of Two-phase flow, Level Set and Two-phase flow, Phase field interface for interface tracking
- Advection equation for interface tracking:

$$\frac{\partial \phi}{\partial t} + \mathbf{u} \cdot \nabla \phi = \nabla \cdot \frac{\mathbf{Y} \lambda}{\epsilon^2} \nabla \psi$$
(For phase-field method)

 $\gamma$  is the mobility (m3·s/kg),  $\lambda$  is the mixing energy density (N) and  $\epsilon$  (m) is the interface thickness parameter and  $\psi$  is referred to as the phase field help variable

- Use of Heat Transfer in Fluids interface and coupled to two-phase flow interface
- Material Properties:

K=(K water-K air )×
$$\varphi$$
 water+K air  
C p=(C water-C air)× $\varphi$  water+C air  
 $\rho$ =( $\rho$  water- $\rho$  air)× $\varphi$  water+ $\rho$  air

K=Thermal conductivity  $C_p = Specific heat capacity$   $\rho = Density$ 





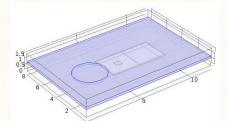
#### Boundary Conditions

Fluid flow

#### Fluid domain

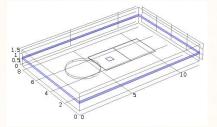


#### Top and bottom surface



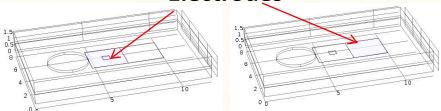
Defined contact angle corresponding to zero voltage (Wetted wall or Navier slip condition

#### Side walls



No slip condition

#### **Electrodes**



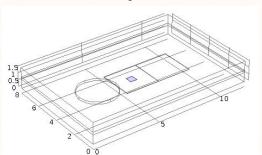
• Defined contact angle corresponding to voltage V(t) (From Young-Lippmann equation) (Wetted wall or Navier slip condition)





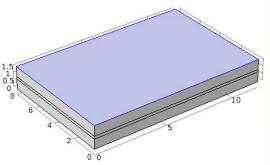
### Boundary Conditions

#### **Hotspot**



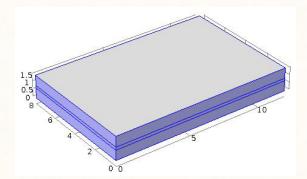
**Heat Transfer** 

#### **Top surface**



Constant heat flux (Boundary heat source)

Other boundaries



Insulated

Convection to air





#### Geometrical dimensions

Parameter name	Dimension (mm)
Electrode dimension	2×2
Channel height	0.1
Hotspot dimension	0.5×0.5
Top & bottom plate thickness	0.7

#### Simulation Parameters

Name	Value
Surface tension, σ	.072 [N/m]
Applied voltage, V <sub>ac</sub>	150[V]
Initial contact angle, $\theta_o$	118[degree]
Dielectric thickness, d	5[μm]
Heat Flux, q"	36.6[W/cm <sup>2</sup> ]
Dielectric constant, $\varepsilon_r$	2.5
Convection co-efficient, h <sub>air</sub>	5[W/(m.K)]
Initial temperature, T	298.15 [K]



## Results



#### **Droplet profiles**

At t=0 ms

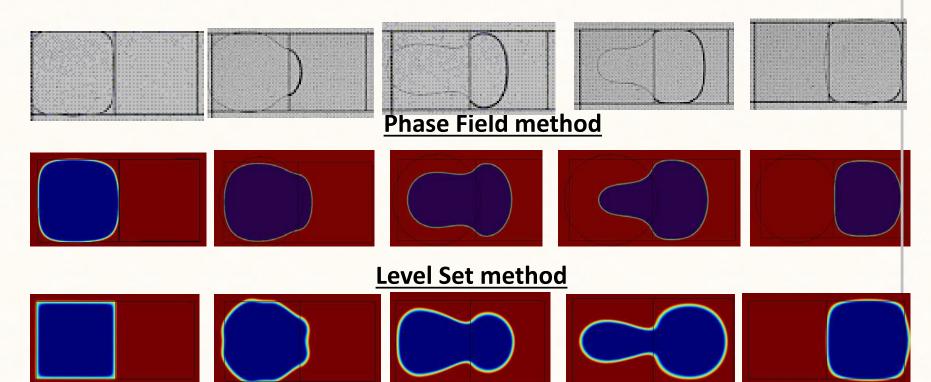
At t=20 ms

At t=40 ms

At t=60 ms

At t=100 ms

#### **Experiment**



• Phase field method gives more accurate and smooth profile

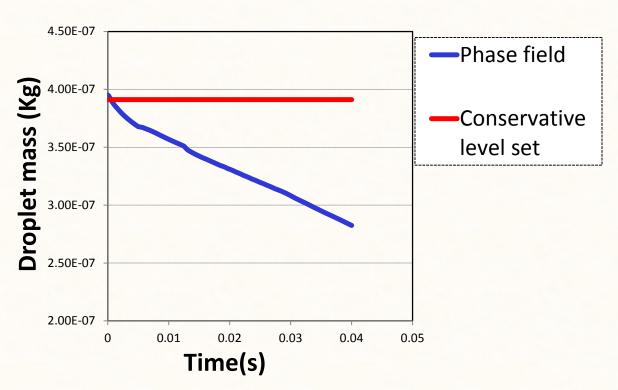
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## Results

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#### Mass conservation issues



- •Phase field: 30% mass loss after 40 ms
- •Conservative level set:
  Guarantees mass
  conservation

- Mass conservation is affected by numerical tuning parameters such as:
  - Mobility tuning parameter
  - Interface thickness
  - Tuning parameter



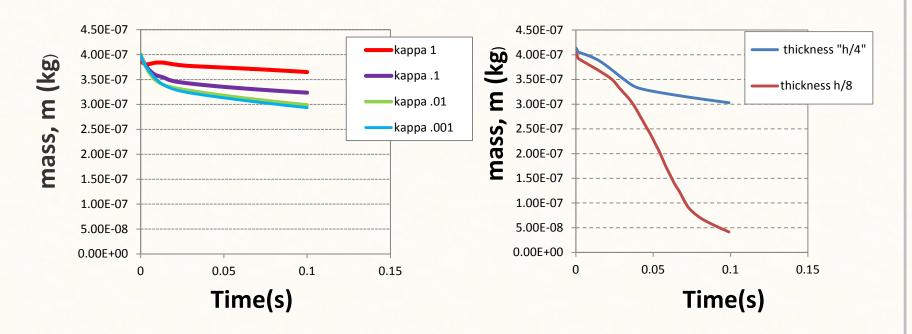
## Results



#### Parametric study for phase field method

#### Mobility tuning parameter, χ

#### Interface thickness, ε



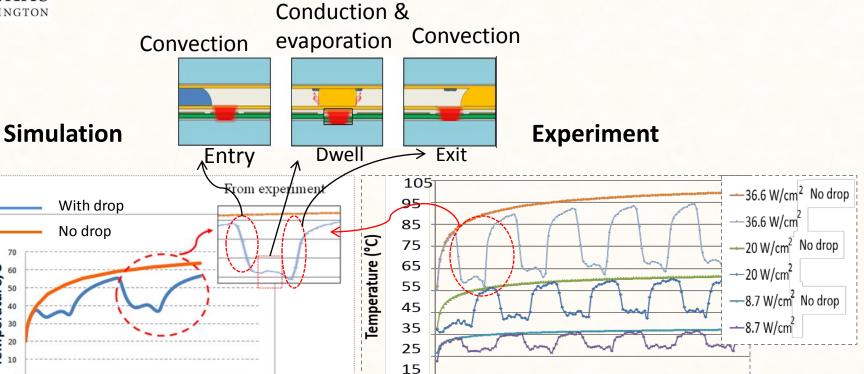
- Mass loss increases with decrease in value of mobility tuning parameter
- Mass loss increases with decrease in interface thickness



# Results Cooling curve of the hotspot

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Time (s)



Average surface temperature of hotspot

• Temperature drop from simulation: 18 °C

Temperature drop in experiment: 20 °C

0.05

0.1

Time, s

0.15

Temperature,



## Conclusions



- 3-Dimensional EWOD droplet motion has been successfully modelled using two methods of interface tracking of two-phase.
  - Two Issues:
    - Mass loss
    - Slight inaccuracy in results due to negligence of hysteresis angle, contact line friction and evaporation heat transfer
- Droplet motion results have been validated with the experiment
- Numerical modeling of cooling of a hotspot has been demonstrated by solving multiphysics problem
- Future study includes modeling heat transfer enhancement due to evaporation by an EWOD actuated droplet



## References



- 1. Shamai, Romi, et al. "Water, electricity, and between... On electrowetting and its applications." *Soft Matter* 4.1 (2008): 38-45.
- 2. A numerical study of microfluidic droplet motions in parallel-plate electrowetting-on-dielectric (EWOD) devices by *Guan, Yin, Ph.D., THE UNIVERSITY OF TEXAS AT ARLINGTON, 2015, 170 pages; 3709722.*
- 3. Chae, Jeong Byung, et al. "3D Electrowetting-on-dielectric Actuation." *Sensors and Actuators A: Physical* (2015).
- 4. Shen, Hsien-Hua, et al. "EWOD microfluidic systems for biomedical applications." *Microfluidics and Nanofluidics* 16.5 (2014): 965-987.
- 5. Olsson, Elin, and Gunilla Kreiss. "A conservative level set method for two phase flow." *Journal of computational physics* 210.1 (2005): 225-246.
- 6. Mohseni, K., and E. S. Baird. "Digitized heat transfer using electrowetting on dielectric." *Nanoscale and Microscale Thermophysical Engineering* 11.1-2 (2007): 99-108.
- 7. Paik, Philip Y., Vamsee K. Pamula, and Krishnendu Chakrabarty. "Adaptive cooling of integrated circuits using digital microfluidics." *Very Large Scale Integration (VLSI) Systems, IEEE Transactions on* 16.4 (2008): 432-443.
- 8. Pollack, Michael G., Richard B. Fair, and Alexander D. Shenderov. "Electrowetting-based actuation of liquid droplets for microfluidic applications." *Applied Physics Letters* 77.11 (2000): 1725-1726.



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