Harnessing Natural Convection in Membraneless Soluble Lead Acid Redox Flow Batteries

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### Vanadium Redox Flow Battery (VRFB)



http://energystorage.org/energy-storage/technologies/vanadium-redox-vrb-flow-batteries

### Soluble Lead Redox Flow Battery (SLRFB)



#### Side Reaction on Anode:

$$PbO + H_2O \xrightarrow{charge} PbO_2 + 2H^+ + 2e^-$$

It's simple and economical!

## **Design Experiments to Probe the Role of Natural Convection**



Without any mixing cell are able to run 40 cycles, why? Or why it is able to charge at constant current?

600

800

400

Time (s)

200

### **Objectives of Work**

Detailed investigation of natural convection in standard and alternative cell designs of SLRFB

> Quantitative experimental validation of predicted flow field



Schematic diagram of standard cell (On wall electrodes cell design)

### **Model Equations**

**Mass Balance Eqn:** 

$$\frac{\partial c_{\cdot}}{\partial t} = -\nabla \cdot N_{i}$$
 Species:  $Pb^{2+}, CH_{3}SO_{3}^{-}, H^{+}$  (1)

**Nernst-Planck Eqn:** 

$$N_i = -D_i \nabla c_i - F z_i c_i u_{m_i} \nabla \phi + c_i u$$
(2)

**Charge Neutrality:** 

$$\sum_{i} z_{i} c_{i} = 0 \tag{3}$$

**Navier-Stokes Eqn:** 

$$\rho \frac{\partial u}{\partial t} + \rho (u \cdot \nabla) u = -\nabla p + \mu \nabla^2 u + \boldsymbol{F}$$
(4)

 $\nabla u = 0$ 

**Buoyancy Force:** 

$$F = \rho g \sum_{i} \beta_{i} (c_{i}^{0} - c_{i})$$
(5)  
**D-eff:** 
$$\beta_{i} = \frac{1}{\rho} \left( \frac{\partial \rho}{\partial c_{i}} \right)_{T,P,c} \int_{j \neq i}$$
(6)

(6)

**Volume Expansion Co-eff:** 

[ Newman & Alyea. Electrochemical system(2004) Bockris & Reddy. Modern Electrochemistry(2006)

### **Initial & Boundary Conditions**

**Overpotential:** 

**Cell Potential:** 



Outlet +ve Electrode -ve Electrode Inlet Walls: No-slip BC

### **Negative Electrode:**

 $2F(N_{Pb}2+.n) = j_{Pb}$  $j_{ca} = j_{Pb}$ 

### Inlet / Outlet:

$$D_i \nabla c_i \cdot n = 0$$
  
j. n = 0  
$$p_{out} = 3 \times 10^5 Pa$$

### **Positive Electrode:**

$$2F(N_{Pb}2+ \cdot n) = j_{Pb}O_{2}$$

$$2F(N_{Pb}O_{2} \cdot n) = j_{Pb}O$$

$$j_{an} = j_{Pb}O_{2} + j_{Pb}O$$
**Initial Condition:**

$$c_{i} = c_{i}^{0}$$

$$c_{s}^{s}PbO_{2} = c_{Pb}^{s}O_{2} = c_{Pb}^{s}O_{2} = 0$$

$$p = 1 \times 10^{5}Pa$$

### Modeling of Standard Cell (on wall electrodes design)



There is a strong electrolyte circulation due to natural convection!

## **Experimental Validation of Flow Field** Using PIV Technique



**Experimental Set-up for Particle Image Velocimetry** 

## Qualitative Validation of Flow Field in Standard Cellstd-15mmFlow prediction: @20s





#### **PIV Experiment**

**Charge Discharge** 

Simulations are able to predict the actual flow pattern!

## Modeling of Lift Cell (off wall electrodes design)



Model is able to predict the observe electrochemical behaviour !

### Effect of Electrodes Splitting on Velocity Field Charging: 20s



Splitting of electrodes improves electrolyte circulation!

### Effect of Electrodes Splitting on Velocity Field Discharging: 20 s



### Splitting of electrodes improves electrolyte circulation!

# Effect of Electrodes Splitting and Staggering on Cell Performance



Splitting and staggering of electrodes into multiple pieces provides better mixing of electrolyte Compared to single piece of electrodes!

## **Effect of External Looping on cell Performance**



External looped cell improves mixing and it performs quite similar to the 6 pieces splitted electrodes design.

### Conclusions

□ Model is able to capture strong natural convection in the cell

- Flow predictions and PIV measurements show good qualitative agreements
- Electrochemical models and experimental data are in good agreement
- Splitting of electrodes into multiple pieces and external looing improves electrolyte mixing and provide charging for longer time

## Thank you! ③