

**COMSOL  
CONFERENCE**  
2018 BANGALORE

# **MODELING AND OPTIMIZATION OF TERAHERTZ-PHOTOCONDUCTIVE ANTENNA (THz-PCA)**

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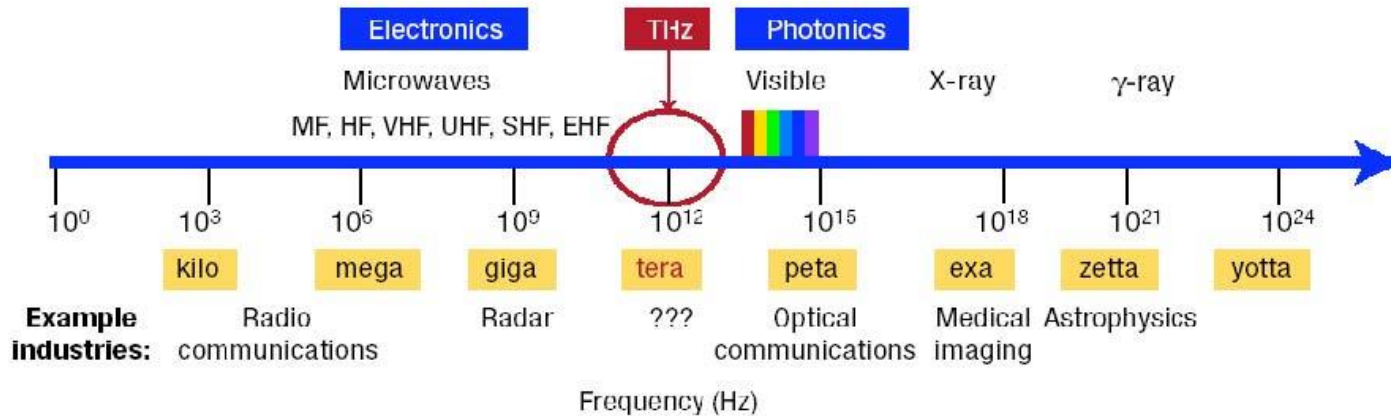


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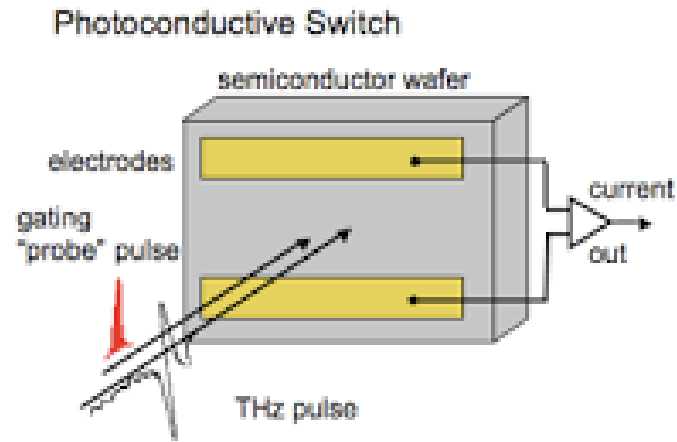
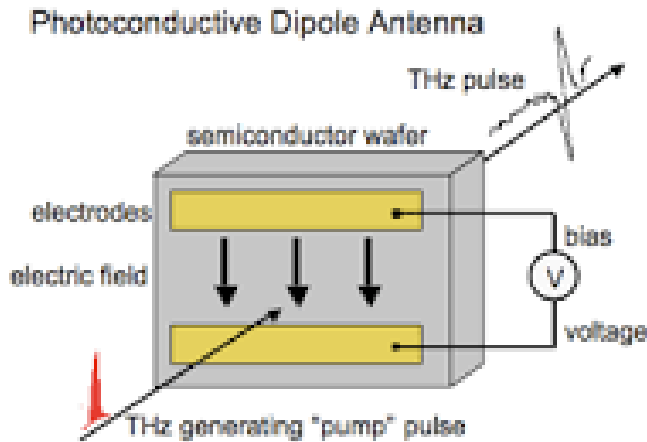
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# INTRODUCTION

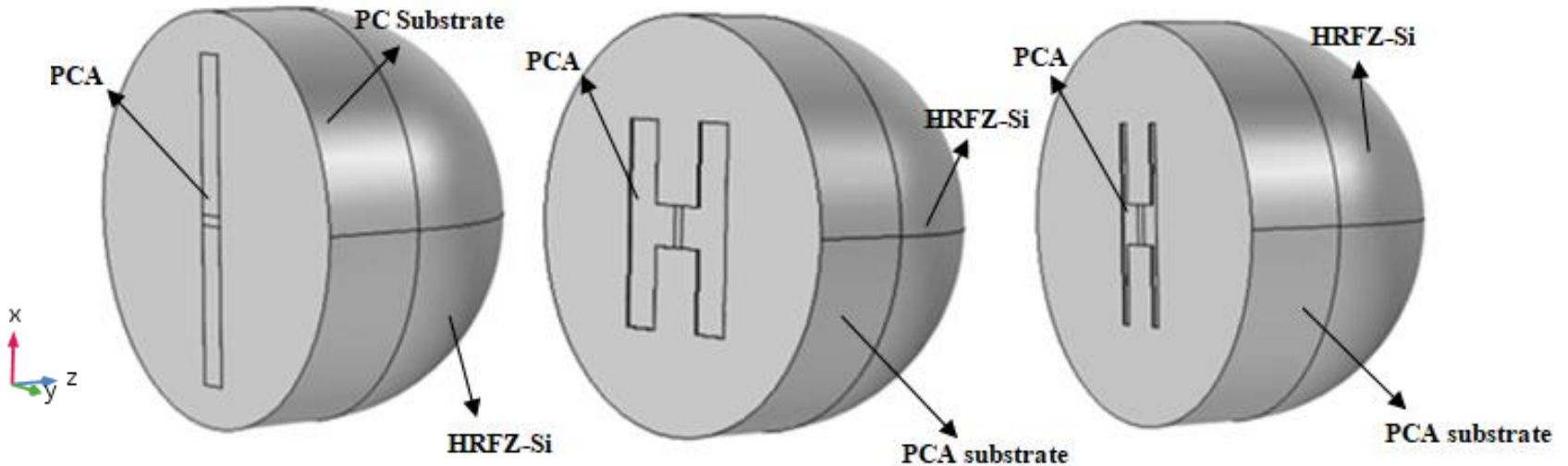


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# MODELLING OF THZ-PCA

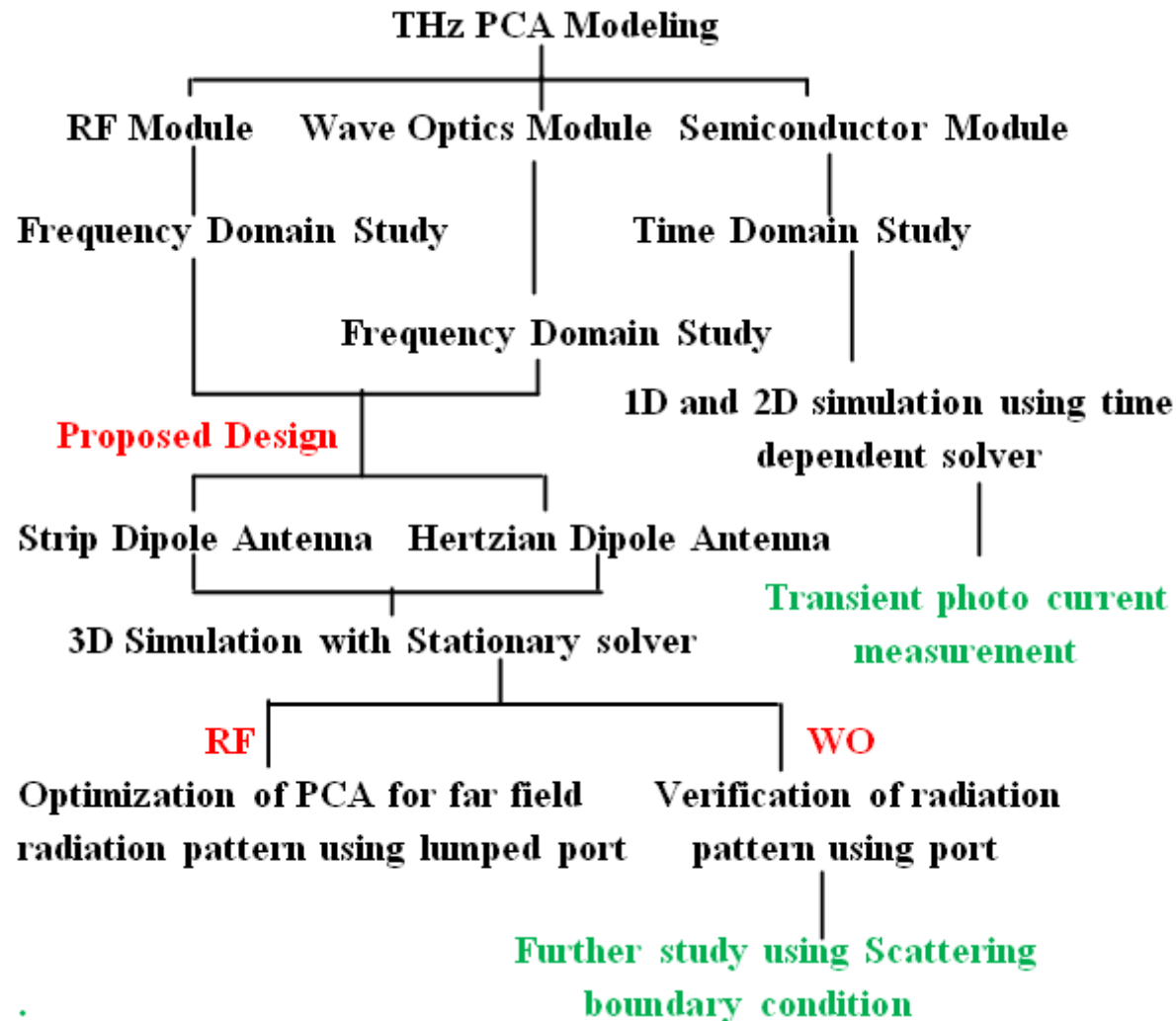


Material	Unit (SI)	Au	LT-GaAs	Si	Air
Property					
Relative permeability	1	1	1	1	1
Relative permittivity	1	-22.5	12.9	11.7	1
Electrical conductivity	S/m	2400	1000	1.5e-6	1.4e-11

$$E_{\text{THz}}(\mathbf{r}, t) = -\frac{1}{4\pi\epsilon_0 c^2} \frac{\partial}{\partial t} \int \frac{J_s\left(\mathbf{r}', t - \frac{|\mathbf{r} - \mathbf{r}'|}{c}\right)}{|\mathbf{r} - \mathbf{r}'|} ds'$$

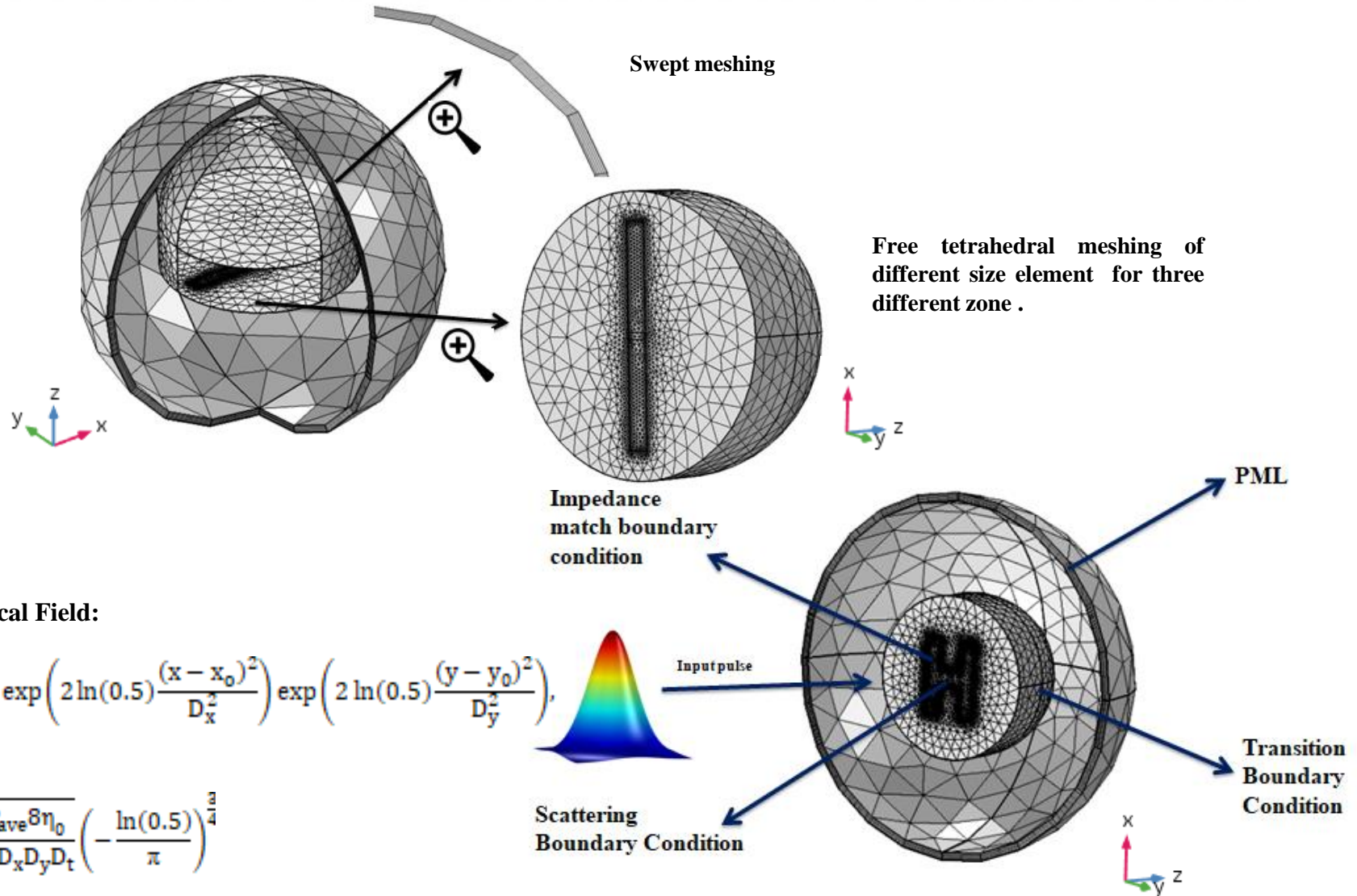


# IMPLEMENTATION WITH COMSOL





# MESHING AND BOUNDARY CONDITION



# SIMULATION

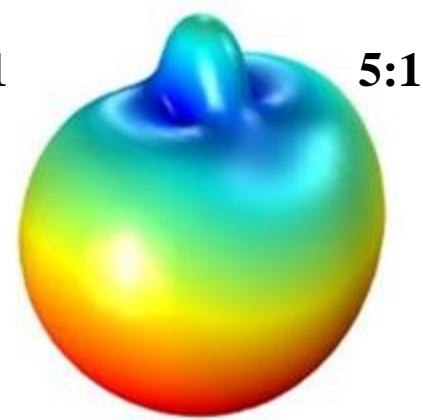
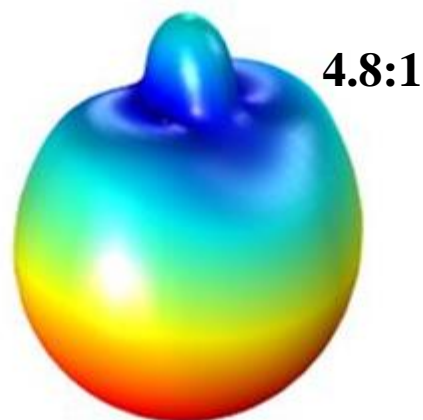
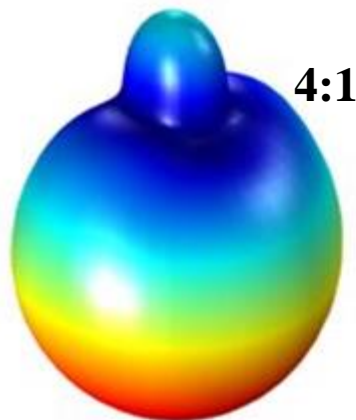
- Optimization
- Optical Response: Solving Maxwell equation using FEM solver
- Electrical Response
- Transient photo-current measurement.

# OPTIMIZED RADIATION PATTERN AND PARAMETER:

THz-PCA Parameter	Strip dipole antenna, Fig. 2(A)	Hertzian dipole antenna, Fig. 2(B)	Hertzian dipole antenna, Fig. 2(C)
$r_{\text{antenna}}(\mu\text{m})$	75.76	93.46	100, 37.5b/w strip
$\text{gap}_{\text{size}}(\mu\text{m})$	19.74	20, monotonic increase with r	20, monotonic increase
$l_{\text{antenna}}(\mu\text{m})$	5	6, monotonic increase with g	3.75
Directivity(dB)	2.9619	3.0019	2.8052

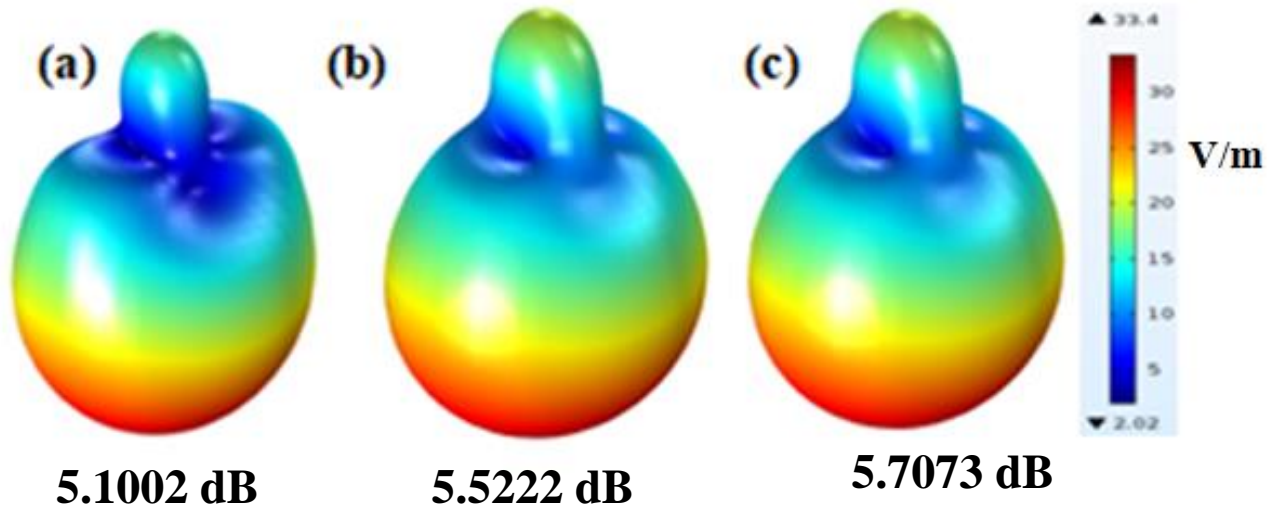
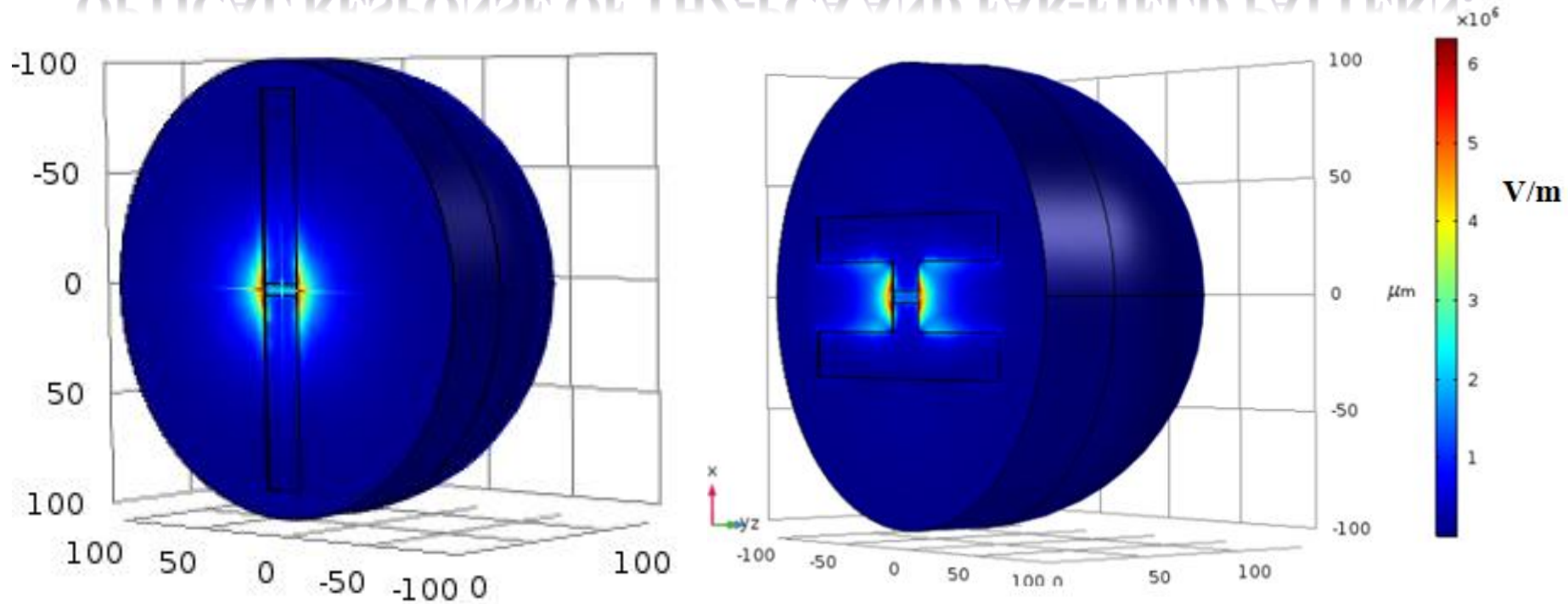
## Optimized Far-field pattern

Aspect ratio:

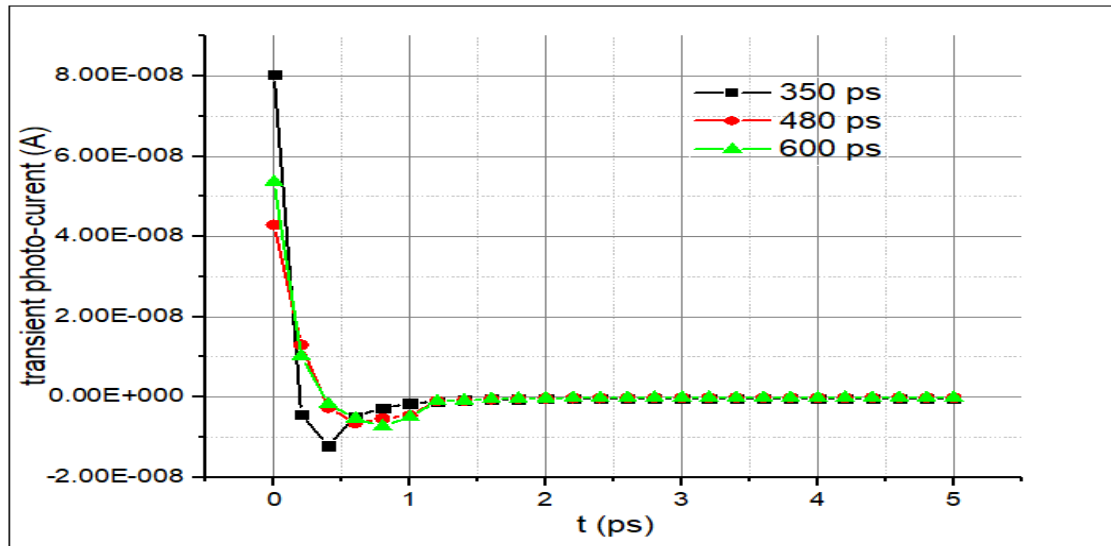
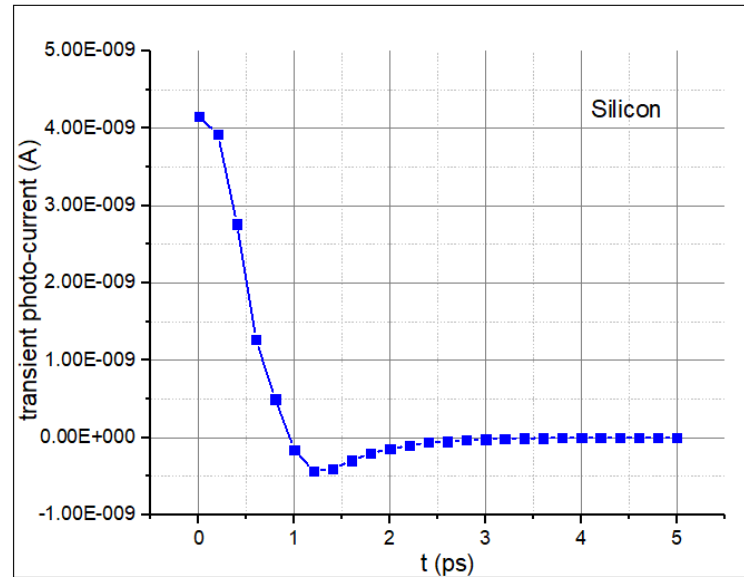
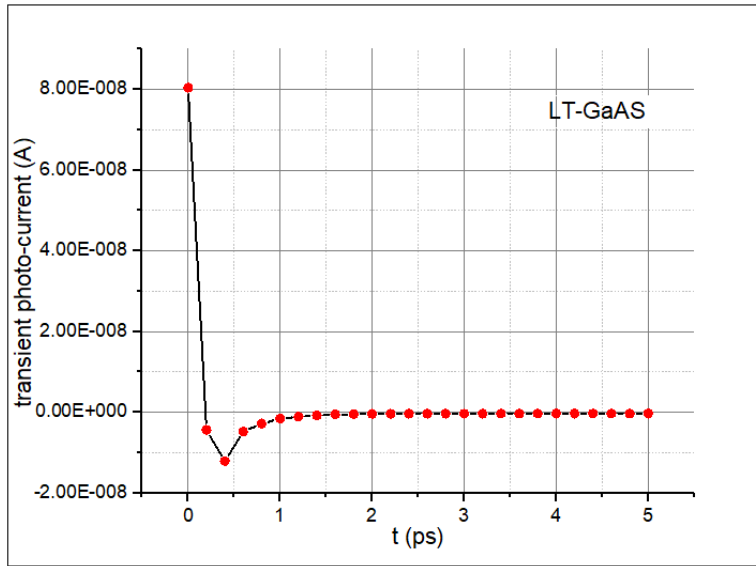




# OPTICAL RESPONSE OF THZ-PCA AND FAR-FIELD PATTERN:



# TRANSIENT PHOTO-CURRENT CALCULATION:



- Summary:**
- The THz-PCA contribute to the compact, inexpensive, low profile future THz wireless communication system.
  - Enhancing the output power, shrinking the size of the systems, enabling high speed frequency sweep and data acquisition.

# REFERENCES

- Fattinger, C., & Grischkowsky, D. (1989). THz beams. *Applied Physics Letters*, 54(6), 490-492
  - Burford, N. M., El-Shenawee, M. O., O'neal, C. B., & Olejniczak, K. J. (2014). THz imaging for nondestructive evaluation of packaged power electronic devices. *Int. J. Emerg. Technol. Adv. Eng*, 4(1), 395-401.
  - Auston, D. H. (1983). Subpicosecond electro-optic shock waves. *Applied Physics Letters*, 43(8), 713-715.
  - Auston, D. H., Cheung, K. P., & Smith, P. R. (1984). Picosecond photoconducting Hertzian dipoles. *Applied physics letters*, 45(3), 284-286.
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**THANK YOU  
FOR YOUR  
ATTENTION**



# Poisson's drift-diffusion equation and Maxwell's equation

$$\epsilon_0 \nabla \cdot (\epsilon_r \nabla V) = q(n - p - N_D + N_A)$$

$$\frac{\partial n}{\partial t} = -\frac{1}{q} \nabla \cdot \left\{ -\mu_n q \nabla (V + \chi) n + \mu_n k_b T G \left( \frac{n}{N_c} \right) \nabla n \right\} - r(x, y, z) + g(x, y, z, t),$$

$$\frac{\partial p}{\partial t} = \frac{1}{q} \nabla \cdot \left\{ -\mu_p q \nabla (V + \chi + E_g) p + \mu_p k_b T G \left( \frac{p}{N_v} \right) \nabla p \right\} - r(x, y, z) + g(x, y, z, t)$$

$$\Delta \times \mu_r^{-1} (\Delta \times \vec{E}) - k_0^2 \left( \epsilon_r - \frac{j\lambda\sigma}{2\pi c \epsilon_r} \right) \vec{E} = 0$$



Symbol	Description	Units	Value
$\epsilon_r$	LT-GaAs	None	12.9
$N_D$	Donor doping concentration	$1/\text{cm}^3$	$1\text{e}16$
$N_A$	Acceptor doping concentration	$1/\text{cm}^3$	0
$\mu_n$	Electron mobility	$\text{m}^2/\text{V}/\text{s}$	0.8
$\mu_p$	Hole mobility	$\text{m}^2/\text{V}/\text{s}$	0.047
$E_g$	Bandgap	V	1.424
$\chi$	Electron affinity	V	4.07
T	Room temperature	K	300
$\tau_n$	SRH electron lifetime	s	$480\text{e}-12$
$\tau_p$	SRH hole lifetime	s	$480\text{e}-12$
$C_n$	Auger electron coefficient	$\text{cm}^6/\text{s}$	$7\text{e}-30$
$C_p$	Auger hole coefficient	$\text{cm}^6/\text{s}$	$7\text{e}-30$
$n_{\text{I,eff}}$	Effective intrinsic carrier concentration	$1/\text{m}^3$	$1.23\text{e}-12$
$V_{\text{bias}}$	Bias Voltage	V	30
$\lambda$	Free space wavelength	nm	800
$P_{\text{ave}}$	Average laser power	mW	3.57
$f_p$	Laser pulse repetition rate	MHz	80
$x_0$	Pulse x-axis center location	$\mu\text{m}$	0
$y_0$	Pulse y-axis center location	$\mu\text{m}$	0
$t_0$	Pulse center location (time)	ps	2
$D_x$	Pulse HPBW (x direction)	$\mu\text{m}$	3
$D_y$	Pulse HPBW (y direction)	$\mu\text{m}$	3
$D_t$	Pulse FWHM (time)	fs	133
$k_{\text{pc}}$	Photoconductor extinction coefficient of LT-GaAs	None	0.0625
$\hat{\mathbf{a}}_e$	$E_{\text{inc}}$ polarization vector	None	$\hat{\mathbf{a}}_x$

$$D_{\text{dB}} = 10 \cdot \log_{10} \left[ \frac{D}{D_{\text{reference}}} \right].$$

$$D = \frac{2}{1 - \cos \frac{\theta}{2}}$$

$$G = 10 \log(\epsilon D)$$

# Directivity

- In [electromagnetics](#), **directivity** is a parameter of an [antenna](#) or [optical system](#) which measures the degree to which the radiation emitted is concentrated in a single direction. It measures the [power density](#) the antenna radiates in the direction of its strongest emission, versus the power density radiated by an ideal [isotropic radiator](#) (which emits uniformly in all directions) radiating the same total power.
- An antenna's directivity is a component of its [gain](#); the other component is its (electrical) [efficiency](#). Directivity is an important measure because many antennas and optical systems are designed to radiate electromagnetic waves in a single direction or over a narrow angle. Directivity is also defined for an antenna receiving electromagnetic waves, and its directivity when receiving is equal to its directivity when transmitting.
- The directivity of an actual antenna can vary from 1.76 dBi for a [short dipole](#), to as much as 50 dBi for a large [dish antenna](#).