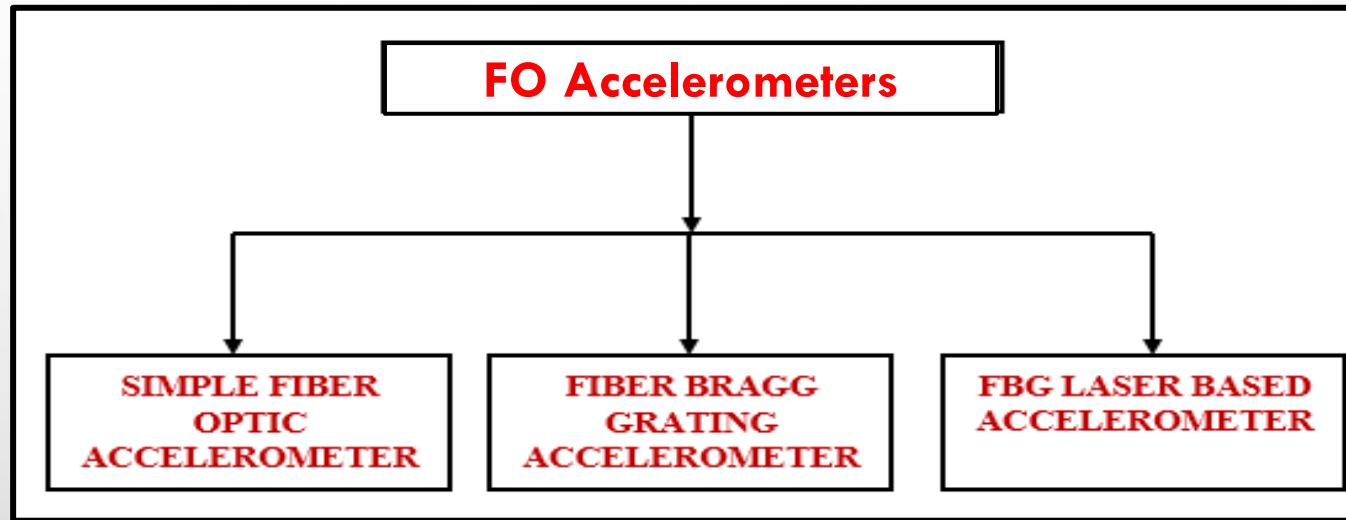


# FEM DESIGN OF INTERFEROMETRIC FBGL ACCELEROMETER FOR UNDERWATER APPLICATIONS

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- FBGL accelerometers offers more sensitivity than FBG accelerometer.
- **Wide range of applications:** including defence, seismic sensing, structural monitoring etc...

Fig. 1 Accelerometer classification

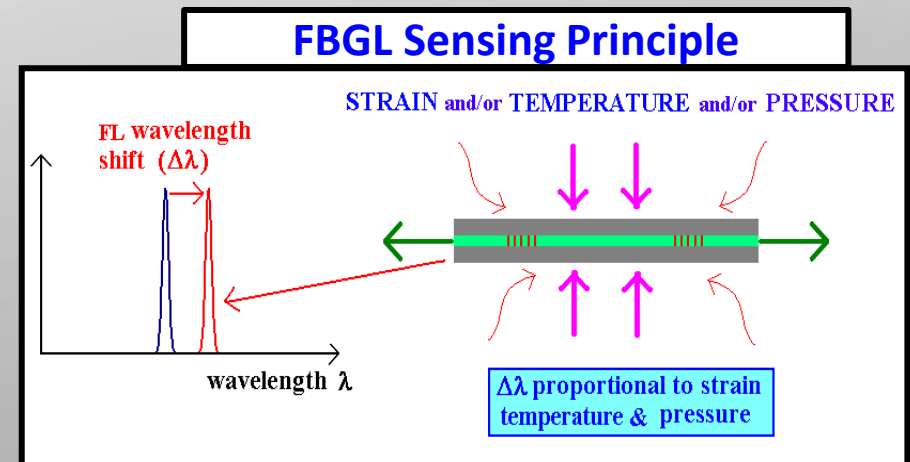
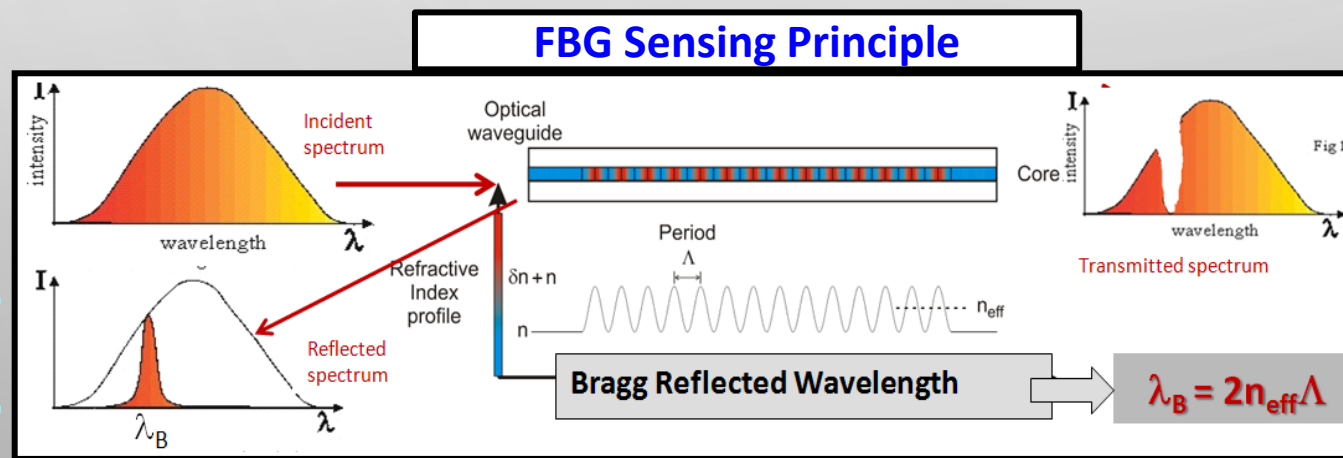


Fig. 2 Shift in Bragg reflected wavelength and Emission wavelength of the laser

# ACCELEROMETER DESIGN

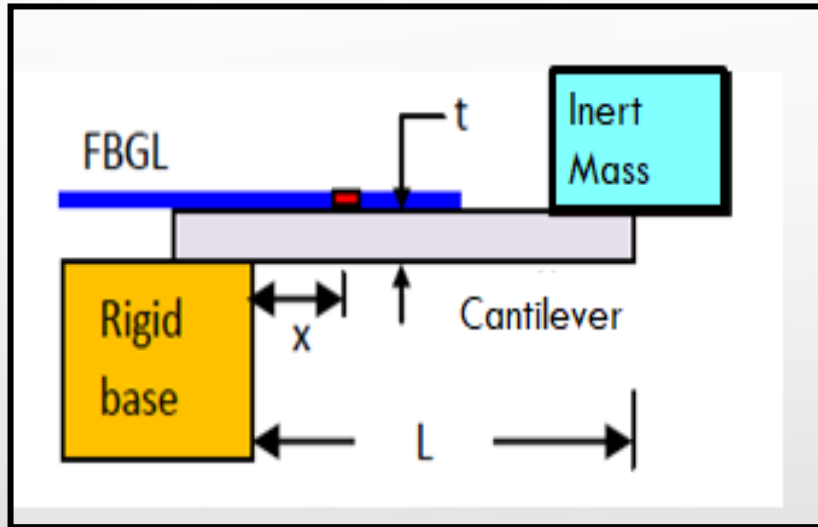


Fig. 3 Proposed Accelerometer Design

$$\text{Resonant frequency, } \omega_0 = \sqrt{\frac{1}{4} \left( \frac{bt^3 E}{ML^3} \right)}$$

- Bandwidth of the accelerometer is determined by the Resonance frequency
- Thump rule: linearity / flat response in dB is  $1/5^{\text{th}}$  of  $\omega_0$

x - Distance of grating from fixed position.

L - Length of cantilever

t - Thickness of cantilever

$L \times b \times t$  - Cantilever dimensions

M - Inert mass

E - Young's modulus

- Strain experienced by the FBG laser,

$$\varepsilon(x) = \frac{3(0.5d)(L-x)}{(\omega_0^2 - \omega^2)L^3} \times a$$

- Sensitivity of the accelerometer

$$S = \frac{\Delta\lambda}{a} = \frac{1.2 \times \varepsilon_F(x)}{a}$$

- Phase sensitivity

$$\frac{\delta(\Delta\phi)}{\delta\lambda_L(\omega)} = \frac{2\pi}{\lambda_L^2} (n \times \Delta L)$$

- FBG laser was used as the sensor instead of simple fiber.
- Along with this system Mach- Zehnder interferometer was used for sensitivity measurement.



- Acceleration of the structure induces dynamic strain along the fiber axis.
- Dynamic strain results in Bragg wavelength shift which is proportional to acceleration.

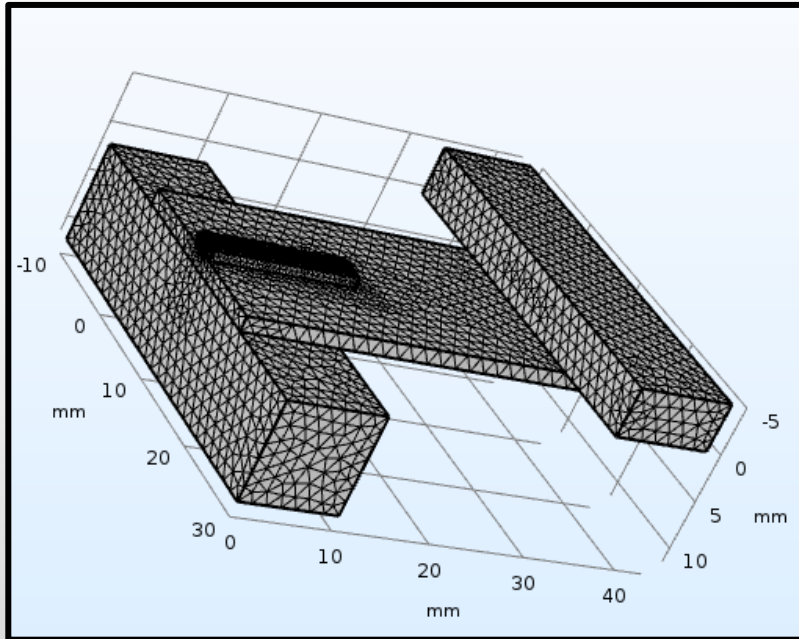


Fig. 4 Meshed configuration of the design

Equations governing the frequency domain study are,

$$-\rho\omega^2 u = \nabla \cdot s + F_v e^{i\phi}, -ik_z = \lambda$$

$$s = s_{ad} + C : \epsilon_{el}, \epsilon_{el} = \epsilon - \epsilon_{inel}$$

$$\epsilon = \frac{1}{2} [(\nabla u)^T + \nabla u]$$

$s$  - stress tensor,

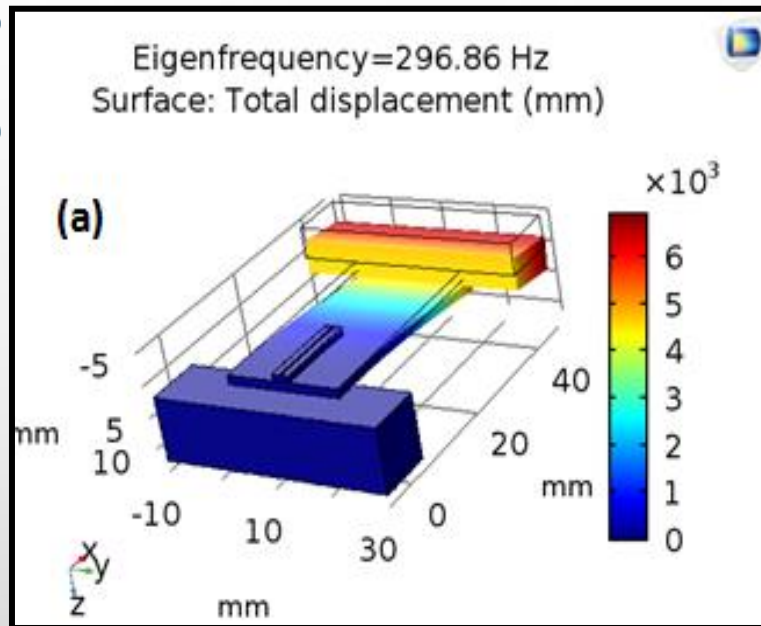
$\epsilon$  - total strain tensor,

$F$  - force

$\omega$  - angular frequency

$\rho$  - density

# Contd...



Resonant mode movement of the cantilever

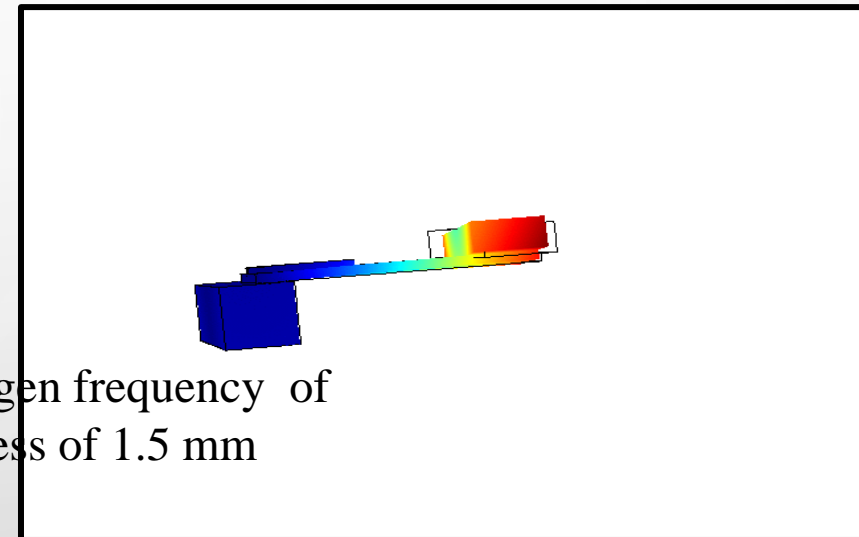


Fig. 5 Results showing Eigen frequency of cantilever with thickness of 1.5 mm

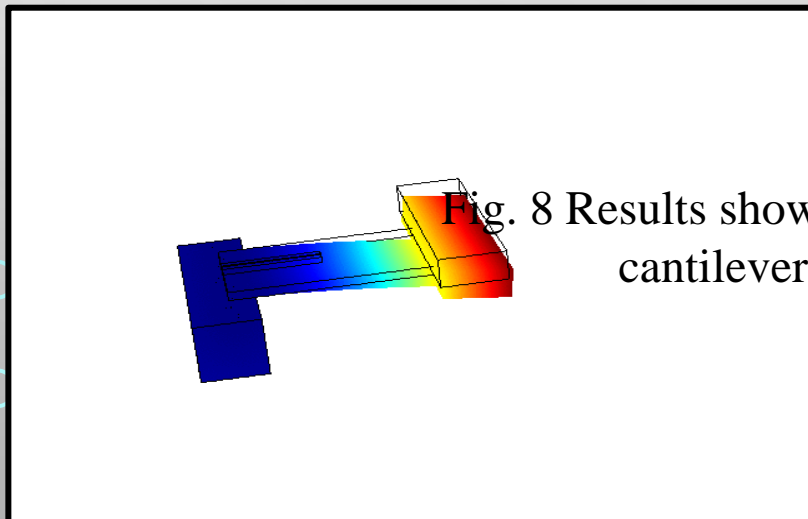
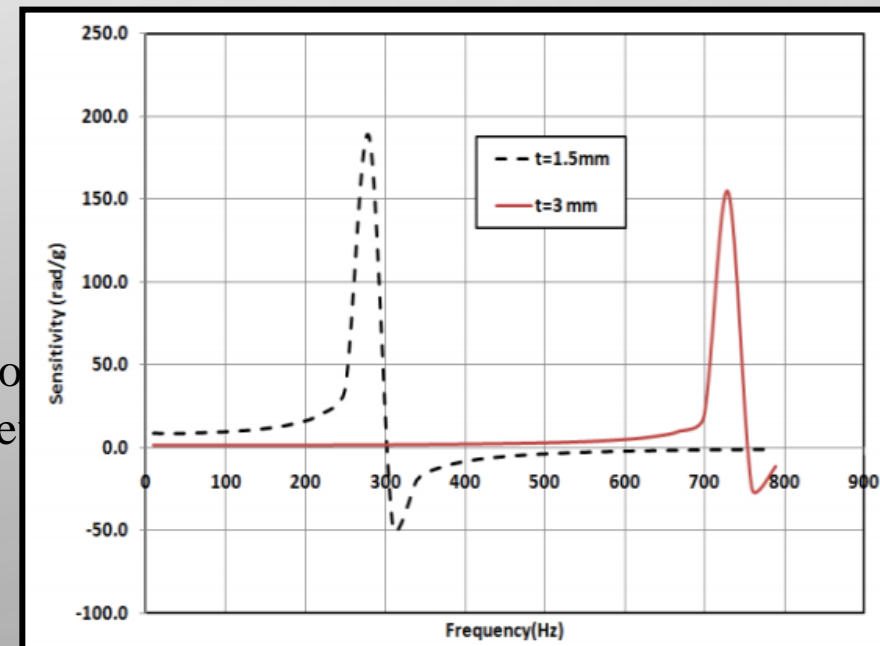


Fig. 8 Results showing dependency of cantilever thickness

Fig. 6 First resonant mode cantilever



# EXPERIMENTAL RESULTS

- Experimental studies were conducted on the prototype developed.

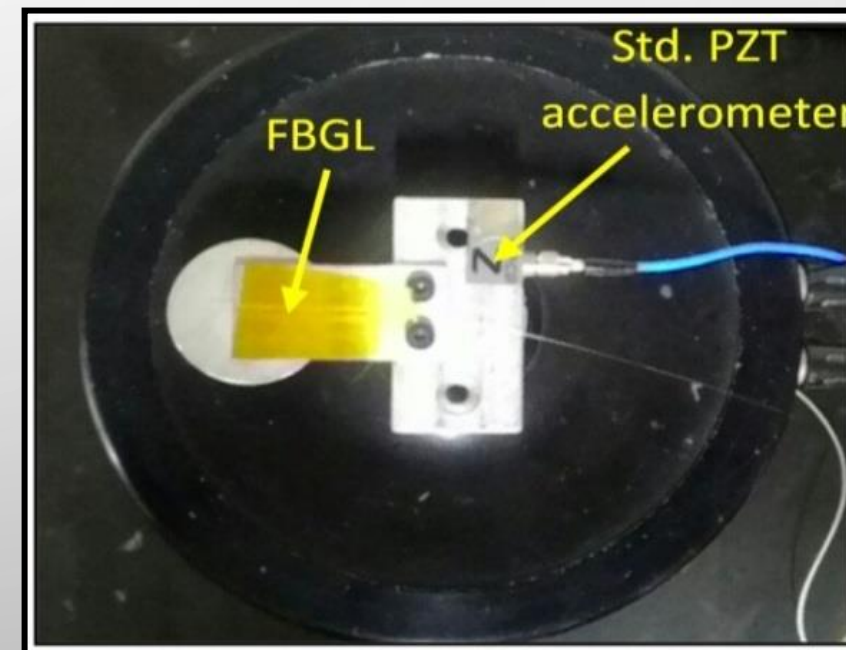
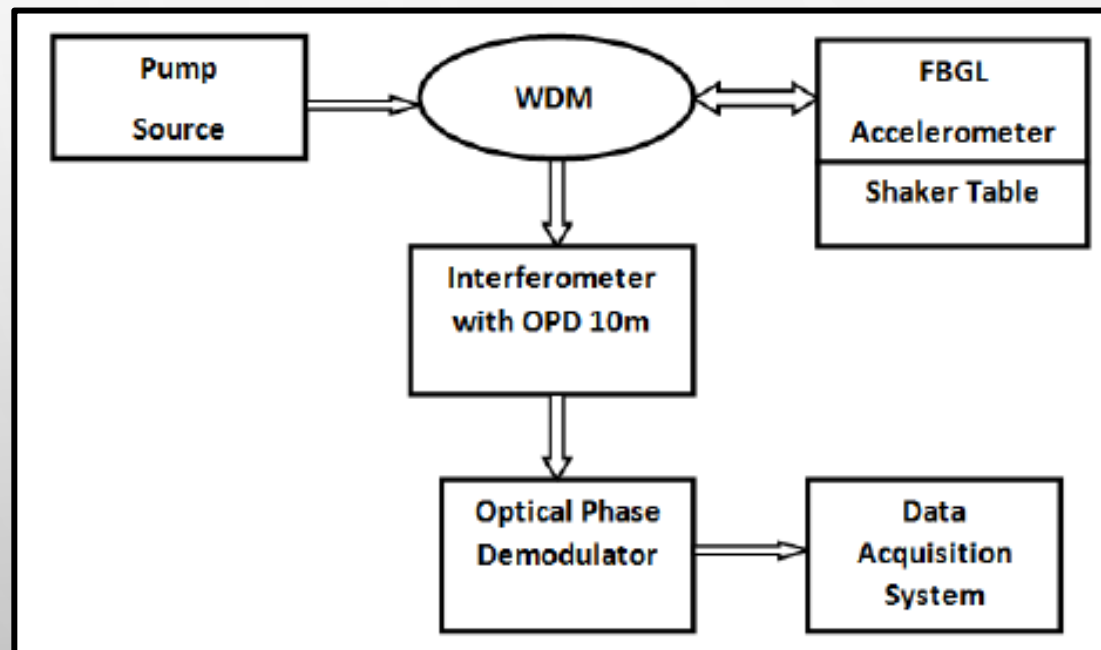


Fig. 9 Experimental setup and block diagram



# Contd...

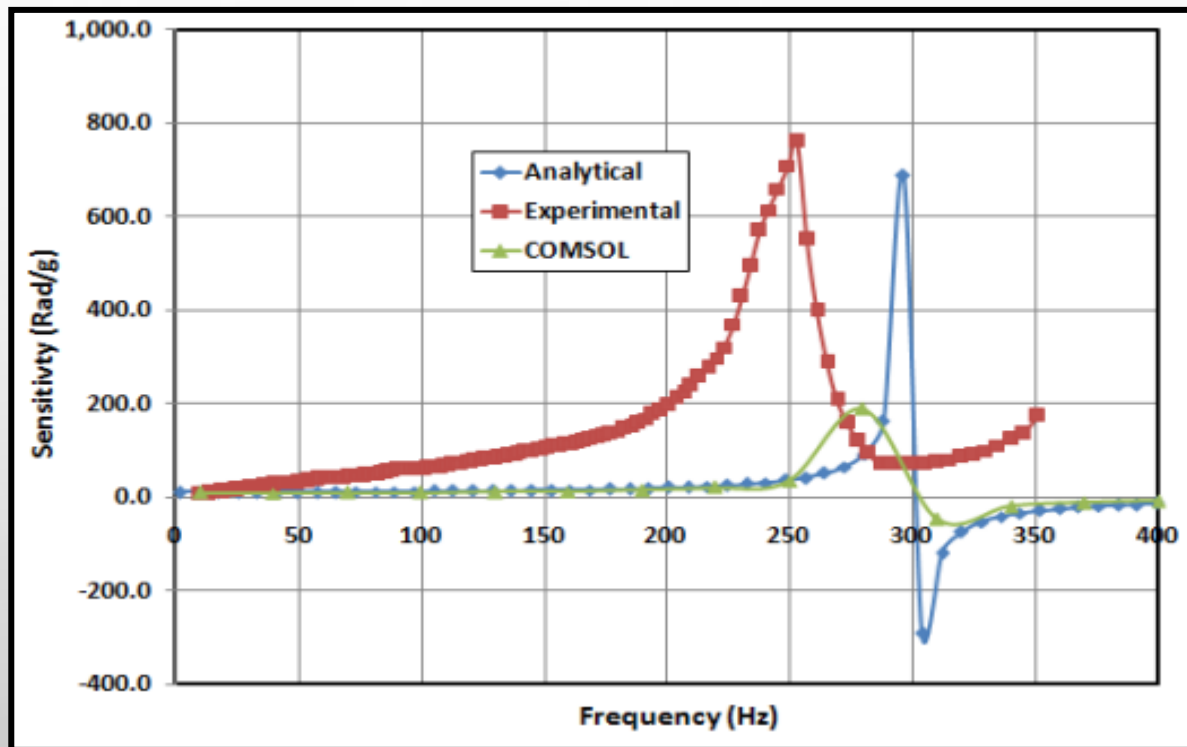


Fig. 10 Comparison between COMSOL, analytical and experimental results.

- Prototype material was selected as stainless steel.
- Dimensions were 40 mm x 20 mm x 1.5 mm.

# CONCLUSION

- Designed prototype yielded a sensitivity of 20V/g (or 20 rad/g) and flatness up to 60Hz.
- FEM modelling of FBGL accelerometer design was carried out along with different cantilever dimensions and materials.
- The COMSOL model results are found to be fairly matching with the analytical and experimental results.

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THANK YOU

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